

# 401 NARRATIVE & SUPPORTING CALCULATIONS

## Briar Chapel Development Great Ridge Parkway Extension

Chatham County, North Carolina

December 14, 2012

Prepared for:



NNP Briar Chapel, LLC  
16 Windy Knoll Circle  
Chapel Hill, North Carolina 27516

Prepared By:



1730 Varsity Drive, Suite 500  
Raleigh, North Carolina 27606  
Phone: (919) 233.8091  
Fax: (919) 233.8031

M&C Project No. 02735-0080



## PROJECT DESCRIPTION

The purpose of the project is to facilitate future residential areas by providing access and roadway connectivity within the development. Great Ridge Parkway Extension will provide a connection from Phase 4 to Granite Mill Boulevard and will provide the thoroughfare around which Briar Chapel South (Phases 7, 8 and 9) will be centered.

Great Ridge Parkway will be comprised of three primary roadway sections as well as the transition zones between each section. These sections will be

- 38' B-B undivided
- 35' B-B undivided
- 2 - 16.5' B-B sections divided.

Based on the conditions of the approved 401 Water Quality Certification, NCDENR-DWQ will require runoff from the roads to be captured and treated for 85% TSS removal before being discharged into the existing stream buffer. To meet this requirement, two BMPs have been designed: a wet detention pond and a level spreader/vegetative filter strip.

Upon completion of the project's construction, the proposed public roads will be turned over to and maintained by NCDOT.

## SITE DESCRIPTION

The project area is approximately 14.5 acres of disturbed area located between the terminus of the existing Great Ridge Parkway within Briar Chapel and at a point along Granite Mill Boulevard near the Margaret B. Pollard Middle School.

The proposed roadway extension will cross a stream that is a direct tributary to Pokeberry Creek (WS-IV; NSW) which is saddled with 100' riparian buffers measured from the top of bank on each side as required by Chatham County. The stream is within the Cape Fear River Basin.

The site generally slopes away from a ridge located near the midpoint of the project area, and drains to the north and south accordingly. The slopes in the site range from 5-20% in localized areas.

## SOILS

According to the Chatham County Generalized Soil Survey, the soils located on the site are classified as Wedowee sandy loam, 2% to 15% slopes (WeC, WeD).

The following soil descriptions are associated with the soils found on the site:

We(X) – Wedowee sandy loam soils are often found in piedmont uplands, along ridges and side slopes. Permeability is moderate and the soils are well drained. Soils have a low shrink/swell potential. The seasonal high water is generally more than 6.0 feet below the surface.

## **WET DETENTION DESIGN**

The wet detention pond on this site has been designed to remove 90% of the total suspended solids entering from the surrounding impervious drainage areas before discharging into the adjacent stream. The calculations provided with this package include all projected future drainage areas that might be captured by the pond. Areas downstream of the ponds exceeded the new slope limitations required by the BMP Manual for level spreaders and vegetated filter strips. Treated runoff will be dissipated by a riprap outlet protection device before entering any stream buffers.

Design parameters were taken from the BMP manual and from DWQ's design supplement forms.

## **LEVEL SPREADER/VEGETATIVE FILTER STRIP DESIGN**

Water quality flows were calculated using methods provided in the NC BMP Manual. For the proposed engineered level spreader/vegetated filter strip devices, the runoff was determined using a 1 in/hr rainfall. The outlet pipe to the level spreader was sized using the runoff. The overflow pipe for events larger than 1 in/hr was set at a higher outlet elevation to ensure that the flows are kept separate.

The LS/VFS system proposed is intended only to be a temporary measure. Upon future buildout, a wet detention pond will be designed to treat runoff from the larger drainage basin and will be designed per the precedence set in other phases of this project.

## **MAINTENANCE CONSIDERATIONS**

The property owner shall be responsible for periodic inspection and maintenance of all temporary erosion control measures devices. Any measure that fails to function as intended shall be repaired immediately.



# POINT PRECIPITATION FREQUENCY ESTIMATES FROM NOAA ATLAS 14



**CHAPEL HILL 2 W, NORTH CAROLINA (31-1677) 35.9086 N 79.0794 W 462 feet**

from "Precipitation Atlas of the United States" NOAA Atlas 14, Volume 2, Version 3

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland, 2004

Extracted: Wed Jan 20 2010

|                   |             |               |             |          |      |      |                     |
|-------------------|-------------|---------------|-------------|----------|------|------|---------------------|
| Confidence Limits | Seasonality | Location Maps | Other Info. | GIS data | Maps | Docs | Return to State Map |
|-------------------|-------------|---------------|-------------|----------|------|------|---------------------|

| <b>Precipitation Intensity Estimates (in/hr)</b> |                       |                        |                        |                        |                        |                         |                      |                      |                       |                       |                       |                       |                       |                        |                        |                        |                        |                        |
|--|-----------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|----------------------|----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| ARI*<br>(years)                                  | <a href="#">5 min</a> | <a href="#">10 min</a> | <a href="#">15 min</a> | <a href="#">30 min</a> | <a href="#">60 min</a> | <a href="#">120 min</a> | <a href="#">3 hr</a> | <a href="#">6 hr</a> | <a href="#">12 hr</a> | <a href="#">24 hr</a> | <a href="#">48 hr</a> | <a href="#">4 day</a> | <a href="#">7 day</a> | <a href="#">10 day</a> | <a href="#">20 day</a> | <a href="#">30 day</a> | <a href="#">45 day</a> | <a href="#">60 day</a> |
| <b>1</b>   | 4.93                  | 3.94                   | 3.28                   | 2.25                   | 1.40                   | 0.84                    | 0.60                 | 0.36                 | 0.21                  | 0.12                  | 0.07                  | 0.04                  | 0.03                  | 0.02                   | 0.01                   | 0.01                   | 0.01                   | 0.01                   |
| <b>2</b>   | 5.81                  | 4.64                   | 3.89                   | 2.69                   | 1.69                   | 1.01                    | 0.72                 | 0.43                 | 0.25                  | 0.15                  | 0.09                  | 0.05                  | 0.03                  | 0.03                   | 0.02                   | 0.01                   | 0.01                   | 0.01                   |
| <b>5</b>   | 6.70                  | 5.36                   | 4.52                   | 3.21                   | 2.06                   | 1.25                    | 0.89                 | 0.53                 | 0.32                  | 0.19                  | 0.11                  | 0.06                  | 0.04                  | 0.03                   | 0.02                   | 0.02                   | 0.01                   | 0.01                   |
| <b>10</b>  | 7.38                  | 5.90                   | 4.98                   | 3.61                   | 2.35                   | 1.43                    | 1.03                 | 0.62                 | 0.37                  | 0.22                  | 0.12                  | 0.07                  | 0.04                  | 0.03                   | 0.02                   | 0.02                   | 0.01                   | 0.01                   |
| <b>25</b>  | 8.11                  | 6.46                   | 5.46                   | 4.04                   | 2.69                   | 1.66                    | 1.20                 | 0.73                 | 0.44                  | 0.25                  | 0.15                  | 0.08                  | 0.05                  | 0.04                   | 0.03                   | 0.02                   | 0.02                   | 0.01                   |
| <b>50</b>  | 8.62                  | 6.86                   | 5.79                   | 4.36                   | 2.95                   | 1.85                    | 1.34                 | 0.82                 | 0.50                  | 0.29                  | 0.16                  | 0.09                  | 0.06                  | 0.04                   | 0.03                   | 0.02                   | 0.02                   | 0.02                   |
| <b>100</b>                                       | 9.07                  | 7.21                   | 6.07                   | 4.65                   | 3.20                   | 2.02                    | 1.48                 | 0.91                 | 0.56                  | 0.32                  | 0.18                  | 0.10                  | 0.06                  | 0.05                   | 0.03                   | 0.02                   | 0.02                   | 0.02                   |
| <b>200</b>                                       | 9.44                  | 7.49                   | 6.30                   | 4.90                   | 3.44                   | 2.20                    | 1.63                 | 1.01                 | 0.62                  | 0.35                  | 0.20                  | 0.11                  | 0.07                  | 0.05                   | 0.03                   | 0.03                   | 0.02                   | 0.02                   |
| <b>500</b>                                       | 9.85                  | 7.79                   | 6.54                   | 5.21                   | 3.73                   | 2.43                    | 1.82                 | 1.14                 | 0.71                  | 0.40                  | 0.22                  | 0.12                  | 0.08                  | 0.06                   | 0.04                   | 0.03                   | 0.02                   | 0.02                   |
| <b>1000</b>                                      | 10.19                 | 8.02                   | 6.71                   | 5.43                   | 3.96                   | 2.62                    | 1.98                 | 1.24                 | 0.78                  | 0.43                  | 0.24                  | 0.13                  | 0.08                  | 0.06                   | 0.04                   | 0.03                   | 0.02                   | 0.02                   |

\* These precipitation frequency estimates are based on a [partial duration series](#). ARI is the Average Recurrence Interval. Please refer to [NOAA Atlas 14 Document](#) for more information. NOTE: Formatting forces estimates near zero to appear as zero.

| <b>* Upper bound of the 90% confidence interval<br/>Precipitation Intensity Estimates (in/hr)</b> |                       |                        |                        |                        |                        |                         |                      |                      |                       |                       |                       |                       |                       |                        |                        |                        |                        |                        |
|---|-----------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|----------------------|----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| ARI**<br>(years)  | <a href="#">5 min</a> | <a href="#">10 min</a> | <a href="#">15 min</a> | <a href="#">30 min</a> | <a href="#">60 min</a> | <a href="#">120 min</a> | <a href="#">3 hr</a> | <a href="#">6 hr</a> | <a href="#">12 hr</a> | <a href="#">24 hr</a> | <a href="#">48 hr</a> | <a href="#">4 day</a> | <a href="#">7 day</a> | <a href="#">10 day</a> | <a href="#">20 day</a> | <a href="#">30 day</a> | <a href="#">45 day</a> | <a href="#">60 day</a> |
| <b>1</b>  | 5.39                  | 4.31                   | 3.59                   | 2.46                   | 1.53                   | 0.92                    | 0.65                 | 0.39                 | 0.23                  | 0.13                  | 0.08                  | 0.04                  | 0.03                  | 0.02                   | 0.01                   | 0.01                   | 0.01                   | 0.01                   |
| <b>2</b>  | 6.36                  | 5.08                   | 4.26                   | 2.94                   | 1.85                   | 1.11                    | 0.79                 | 0.47                 | 0.28                  | 0.16                  | 0.09                  | 0.05                  | 0.03                  | 0.03                   | 0.02                   | 0.01                   | 0.01                   | 0.01                   |
| <b>5</b>  | 7.31                  | 5.86                   | 4.94                   | 3.51                   | 2.25                   | 1.37                    | 0.97                 | 0.58                 | 0.34                  | 0.20                  | 0.12                  | 0.06                  | 0.04                  | 0.03                   | 0.02                   | 0.02                   | 0.01                   | 0.01                   |
| <b>10</b>   | 8.06                  | 6.44                   | 5.43                   | 3.94                   | 2.56                   | 1.57                    | 1.12                 | 0.68                 | 0.40                  | 0.23                  | 0.13                  | 0.07                  | 0.05                  | 0.04                   | 0.02                   | 0.02                   | 0.02                   | 0.01                   |
| <b>25</b>   | 8.83                  | 7.04                   | 5.95                   | 4.41                   | 2.93                   | 1.82                    | 1.31                 | 0.79                 | 0.48                  | 0.27                  | 0.16                  | 0.09                  | 0.05                  | 0.04                   | 0.03                   | 0.02                   | 0.02                   | 0.01                   |
| <b>50</b>   | 9.38                  | 7.48                   | 6.31                   | 4.75                   | 3.22                   | 2.02                    | 1.47                 | 0.89                 | 0.54                  | 0.31                  | 0.17                  | 0.10                  | 0.06                  | 0.05                   | 0.03                   | 0.02                   | 0.02                   | 0.02                   |
| <b>100</b>  | 9.89                  | 7.85                   | 6.62                   | 5.07                   | 3.49                   | 2.22                    | 1.62                 | 0.99                 | 0.60                  | 0.34                  | 0.19                  | 0.11                  | 0.07                  | 0.05                   | 0.03                   | 0.02                   | 0.02                   | 0.02                   |
| <b>200</b>  | 10.32                 | 8.18                   | 6.88                   | 5.35                   | 3.75                   | 2.41                    | 1.78                 | 1.09                 | 0.67                  | 0.38                  | 0.21                  | 0.12                  | 0.07                  | 0.06                   | 0.04                   | 0.03                   | 0.02                   | 0.02                   |
| <b>500</b>  | 10.78                 | 8.52                   | 7.15                   | 5.69                   | 4.08                   | 2.66                    | 1.99                 | 1.23                 | 0.76                  | 0.43                  | 0.24                  | 0.13                  | 0.08                  | 0.06                   | 0.04                   | 0.03                   | 0.02                   | 0.02                   |
| <b>1000</b>   | 11.14                 | 8.77                   | 7.34                   | 5.94                   | 4.34                   | 2.87                    | 2.16                 | 1.36                 | 0.85                  | 0.46                  | 0.26                  | 0.14                  | 0.09                  | 0.07                   | 0.04                   | 0.03                   | 0.02                   | 0.02                   |

\* The upper bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are greater than.

\*\* These precipitation frequency estimates are based on a [partial duration series](#). ARI is the Average Recurrence Interval. Please refer to [NOAA Atlas 14 Document](#) for more information. NOTE: Formatting prevents estimates near zero to appear as zero.

| <b>* Lower bound of the 90% confidence interval<br/>Precipitation Intensity Estimates (in/hr)</b> |                       |                        |                        |                        |                        |                         |                      |                      |                       |                       |                       |                       |                       |                        |                        |                        |                        |                        |
|---|-----------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|----------------------|----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| ARI**<br>(years)  | <a href="#">5 min</a> | <a href="#">10 min</a> | <a href="#">15 min</a> | <a href="#">30 min</a> | <a href="#">60 min</a> | <a href="#">120 min</a> | <a href="#">3 hr</a> | <a href="#">6 hr</a> | <a href="#">12 hr</a> | <a href="#">24 hr</a> | <a href="#">48 hr</a> | <a href="#">4 day</a> | <a href="#">7 day</a> | <a href="#">10 day</a> | <a href="#">20 day</a> | <a href="#">30 day</a> | <a href="#">45 day</a> | <a href="#">60 day</a> |
| <b>1</b>  | 4.93                  | 3.94                   | 3.28                   | 2.25                   | 1.40                   | 0.84                    | 0.60                 | 0.36                 | 0.21                  | 0.12                  | 0.07                  | 0.04                  | 0.03                  | 0.02                   | 0.01                   | 0.01                   | 0.01                   | 0.01                   |
| <b>2</b>  | 5.81                  | 4.64                   | 3.89                   | 2.69                   | 1.69                   | 1.01                    | 0.72                 | 0.43                 | 0.25                  | 0.15                  | 0.09                  | 0.05                  | 0.03                  | 0.03                   | 0.02                   | 0.01                   | 0.01                   | 0.01                   |
| <b>5</b>  | 6.70                  | 5.36                   | 4.52                   | 3.21                   | 2.06                   | 1.25                    | 0.89                 | 0.53                 | 0.32                  | 0.19                  | 0.11                  | 0.06                  | 0.04                  | 0.03                   | 0.02                   | 0.02                   | 0.01                   | 0.01                   |
| <b>10</b>   | 7.38                  | 5.90                   | 4.98                   | 3.61                   | 2.35                   | 1.43                    | 1.03                 | 0.62                 | 0.37                  | 0.22                  | 0.12                  | 0.07                  | 0.04                  | 0.03                   | 0.02                   | 0.02                   | 0.01                   | 0.01                   |
| <b>25</b>   | 8.11                  | 6.46                   | 5.46                   | 4.04                   | 2.69                   | 1.66                    | 1.20                 | 0.73                 | 0.44                  | 0.25                  | 0.15                  | 0.08                  | 0.05                  | 0.04                   | 0.03                   | 0.02                   | 0.02                   | 0.01                   |
| <b>50</b>   | 8.62                  | 6.86                   | 5.79                   | 4.36                   | 2.95                   | 1.85                    | 1.34                 | 0.82                 | 0.50                  | 0.29                  | 0.16                  | 0.09                  | 0.06                  | 0.04                   | 0.03                   | 0.02                   | 0.02                   | 0.02                   |
| <b>100</b>  | 9.07                  | 7.21                   | 6.07                   | 4.65                   | 3.20                   | 2.02                    | 1.48                 | 0.91                 | 0.56                  | 0.32                  | 0.18                  | 0.10                  | 0.06                  | 0.05                   | 0.03                   | 0.02                   | 0.02                   | 0.02                   |
| <b>200</b>  | 9.44                  | 7.49                   | 6.30                   | 4.90                   | 3.44                   | 2.20                    | 1.63                 | 1.01                 | 0.62                  | 0.35                  | 0.20                  | 0.11                  | 0.07                  | 0.05                   | 0.03                   | 0.03                   | 0.02                   | 0.02                   |
| <b>500</b>  | 9.85                  | 7.79                   | 6.54                   | 5.21                   | 3.73                   | 2.43                    | 1.82                 | 1.14                 | 0.71                  | 0.40                  | 0.22                  | 0.12                  | 0.08                  | 0.06                   | 0.04                   | 0.03                   | 0.02                   | 0.02                   |
| <b>1000</b>   | 10.19                 | 8.02                   | 6.71                   | 5.43                   | 3.96                   | 2.62                    | 1.98                 | 1.24                 | 0.78                  | 0.43                  | 0.24                  | 0.13                  | 0.08                  | 0.06                   | 0.04                   | 0.03                   | 0.02                   | 0.02                   |



# POINT PRECIPITATION FREQUENCY ESTIMATES FROM NOAA ATLAS 14



**CHAPEL HILL 2 W, NORTH CAROLINA (31-1677) 35.9086 N 79.0794 W 462 feet**

from "Precipitation Atlas of the United States" NOAA Atlas 14, Volume 2, Version 3

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland, 2004

Extracted: Tue Jan 19 2010

|                   |             |               |             |          |      |      |                     |
|-------------------|-------------|---------------|-------------|----------|------|------|---------------------|
| Confidence Limits | Seasonality | Location Maps | Other Info. | GIS data | Maps | Docs | Return to State Map |
|-------------------|-------------|---------------|-------------|----------|------|------|---------------------|

| <b>Precipitation Frequency Estimates (inches)</b> |                       |                        |                        |                        |                        |                         |                      |                      |                       |                       |                       |                       |                       |                        |                        |                        |                        |                        |
|---|-----------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|----------------------|----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| ARI*<br>(years)                                   | <a href="#">5 min</a> | <a href="#">10 min</a> | <a href="#">15 min</a> | <a href="#">30 min</a> | <a href="#">60 min</a> | <a href="#">120 min</a> | <a href="#">3 hr</a> | <a href="#">6 hr</a> | <a href="#">12 hr</a> | <a href="#">24 hr</a> | <a href="#">48 hr</a> | <a href="#">4 day</a> | <a href="#">7 day</a> | <a href="#">10 day</a> | <a href="#">20 day</a> | <a href="#">30 day</a> | <a href="#">45 day</a> | <a href="#">60 day</a> |
| 1   | 0.41                  | 0.66                   | 0.82                   | 1.12                   | 1.40                   | 1.68                    | 1.79                 | 2.15                 | 2.54                  | 2.96                  | 3.46                  | 3.87                  | 4.44                  | 5.05                   | 6.76                   | 8.39                   | 10.69                  | 12.84                  |
| 2   | 0.48                  | 0.77                   | 0.97                   | 1.34                   | 1.69                   | 2.02                    | 2.16                 | 2.59                 | 3.06                  | 3.58                  | 4.17                  | 4.64                  | 5.30                  | 6.00                   | 7.97                   | 9.88                   | 12.52                  | 14.97                  |
| 5   | 0.56                  | 0.89                   | 1.13                   | 1.60                   | 2.06                   | 2.49                    | 2.66                 | 3.20                 | 3.80                  | 4.47                  | 5.17                  | 5.71                  | 6.44                  | 7.21                   | 9.41                   | 11.47                  | 14.32                  | 16.89                  |
| 10  | 0.61                  | 0.98                   | 1.25                   | 1.80                   | 2.35                   | 2.87                    | 3.08                 | 3.71                 | 4.44                  | 5.17                  | 5.95                  | 6.54                  | 7.34                  | 8.15                   | 10.56                  | 12.72                  | 15.72                  | 18.37                  |
| 25  | 0.68                  | 1.08                   | 1.36                   | 2.02                   | 2.69                   | 3.33                    | 3.61                 | 4.37                 | 5.28                  | 6.11                  | 6.99                  | 7.68                  | 8.57                  | 9.42                   | 12.11                  | 14.36                  | 17.55                  | 20.28                  |
| 50  | 0.72                  | 1.14                   | 1.45                   | 2.18                   | 2.95                   | 3.70                    | 4.04                 | 4.92                 | 5.99                  | 6.86                  | 7.81                  | 8.57                  | 9.54                  | 10.43                  | 13.34                  | 15.62                  | 18.95                  | 21.72                  |
| 100   | 0.76                  | 1.20                   | 1.52                   | 2.33                   | 3.20                   | 4.05                    | 4.46                 | 5.47                 | 6.71                  | 7.62                  | 8.64                  | 9.49                  | 10.53                 | 11.44                  | 14.57                  | 16.87                  | 20.31                  | 23.11                  |
| 200   | 0.79                  | 1.25                   | 1.57                   | 2.45                   | 3.44                   | 4.40                    | 4.89                 | 6.03                 | 7.47                  | 8.41                  | 9.49                  | 10.44                 | 11.56                 | 12.47                  | 15.83                  | 18.12                  | 21.67                  | 24.46                  |
| 500   | 0.82                  | 1.30                   | 1.64                   | 2.60                   | 3.73                   | 4.86                    | 5.46                 | 6.80                 | 8.53                  | 9.50                  | 10.66                 | 11.73                 | 12.96                 | 13.87                  | 17.55                  | 19.80                  | 23.46                  | 26.21                  |
| 1000  | 0.85                  | 1.34                   | 1.68                   | 2.72                   | 3.96                   | 5.23                    | 5.93                 | 7.44                 | 9.43                  | 10.35                 | 11.58                 | 12.76                 | 14.06                 | 14.97                  | 18.89                  | 21.09                  | 24.83                  | 27.53                  |

\* These precipitation frequency estimates are based on a [partial duration series](#). ARI is the Average Recurrence Interval. Please refer to [NOAA Atlas 14 Document](#) for more information. NOTE: Formatting forces estimates near zero to appear as zero.

| <b>* Upper bound of the 90% confidence interval<br/>Precipitation Frequency Estimates (inches)</b> |                       |                        |                        |                        |                        |                         |                      |                      |                       |                       |                       |                       |                       |                        |                        |                        |                        |                        |
|--|-----------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|----------------------|----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| ARI**<br>(years)   | <a href="#">5 min</a> | <a href="#">10 min</a> | <a href="#">15 min</a> | <a href="#">30 min</a> | <a href="#">60 min</a> | <a href="#">120 min</a> | <a href="#">3 hr</a> | <a href="#">6 hr</a> | <a href="#">12 hr</a> | <a href="#">24 hr</a> | <a href="#">48 hr</a> | <a href="#">4 day</a> | <a href="#">7 day</a> | <a href="#">10 day</a> | <a href="#">20 day</a> | <a href="#">30 day</a> | <a href="#">45 day</a> | <a href="#">60 day</a> |
| 1  | 0.45                  | 0.72                   | 0.90                   | 1.23                   | 1.53                   | 1.84                    | 1.96                 | 2.35                 | 2.77                  | 3.16                  | 3.70                  | 4.14                  | 4.73                  | 5.37                   | 7.14                   | 8.87                   | 11.24                  | 13.44                  |
| 2  | 0.53                  | 0.85                   | 1.06                   | 1.47                   | 1.85                   | 2.22                    | 2.37                 | 2.83                 | 3.34                  | 3.82                  | 4.46                  | 4.96                  | 5.64                  | 6.38                   | 8.43                   | 10.42                  | 13.15                  | 15.68                  |
| 5  | 0.61                  | 0.98                   | 1.23                   | 1.75                   | 2.25                   | 2.73                    | 2.92                 | 3.50                 | 4.15                  | 4.77                  | 5.53                  | 6.09                  | 6.86                  | 7.66                   | 9.95                   | 12.10                  | 15.04                  | 17.69                  |
| 10   | 0.67                  | 1.07                   | 1.36                   | 1.97                   | 2.56                   | 3.14                    | 3.37                 | 4.05                 | 4.83                  | 5.51                  | 6.36                  | 6.99                  | 7.82                  | 8.66                   | 11.17                  | 13.41                  | 16.51                  | 19.25                  |
| 25   | 0.74                  | 1.17                   | 1.49                   | 2.20                   | 2.93                   | 3.64                    | 3.94                 | 4.76                 | 5.73                  | 6.54                  | 7.47                  | 8.22                  | 9.14                  | 10.02                  | 12.82                  | 15.15                  | 18.44                  | 21.26                  |
| 50   | 0.78                  | 1.25                   | 1.58                   | 2.38                   | 3.22                   | 4.04                    | 4.41                 | 5.35                 | 6.47                  | 7.34                  | 8.35                  | 9.19                  | 10.19                 | 11.11                  | 14.14                  | 16.50                  | 19.92                  | 22.80                  |
| 100  | 0.82                  | 1.31                   | 1.66                   | 2.53                   | 3.49                   | 4.43                    | 4.87                 | 5.94                 | 7.25                  | 8.17                  | 9.27                  | 10.19                 | 11.26                 | 12.21                  | 15.48                  | 17.85                  | 21.39                  | 24.28                  |
| 200  | 0.86                  | 1.36                   | 1.72                   | 2.68                   | 3.75                   | 4.82                    | 5.34                 | 6.56                 | 8.06                  | 9.03                  | 10.19                 | 11.22                 | 12.38                 | 13.33                  | 16.86                  | 19.21                  | 22.85                  | 25.73                  |
| 500  | 0.90                  | 1.42                   | 1.79                   | 2.84                   | 4.08                   | 5.32                    | 5.96                 | 7.39                 | 9.20                  | 10.21                 | 11.47                 | 12.65                 | 13.91                 | 14.86                  | 18.72                  | 21.04                  | 24.81                  | 27.63                  |
| 1000   | 0.93                  | 1.46                   | 1.83                   | 2.97                   | 4.34                   | 5.74                    | 6.50                 | 8.11                 | 10.19                 | 11.15                 | 12.49                 | 13.79                 | 15.14                 | 16.07                  | 20.20                  | 22.46                  | 26.31                  | 29.07                  |

\* The upper bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are greater than.

\*\* These precipitation frequency estimates are based on a [partial duration series](#). ARI is the Average Recurrence Interval. Please refer to [NOAA Atlas 14 Document](#) for more information. NOTE: Formatting prevents estimates near zero to appear as zero.

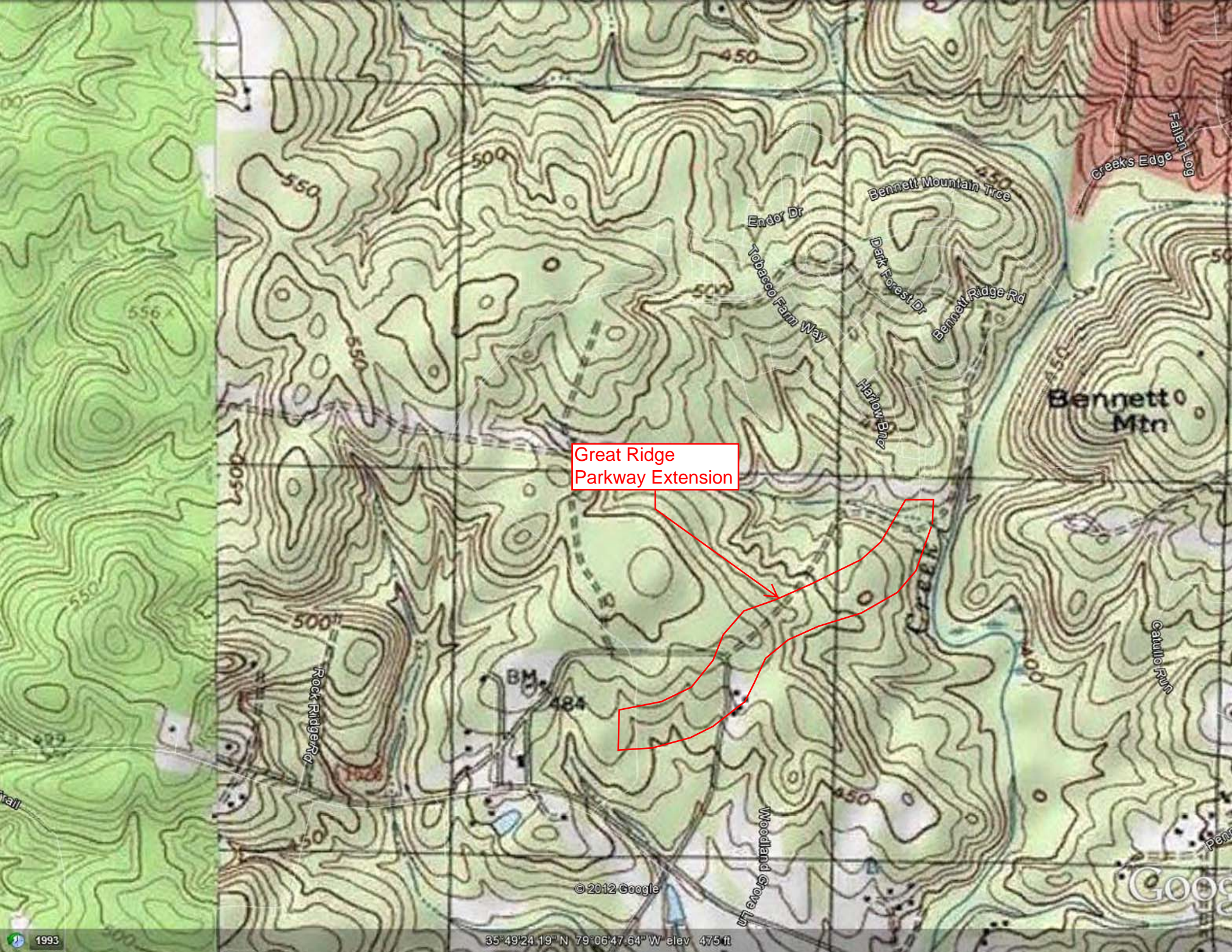
| <b>* Lower bound of the 90% confidence interval<br/>Precipitation Frequency Estimates (inches)</b> |                       |                        |                        |                        |                        |                         |                      |                      |                       |                       |                       |                       |                       |                        |                        |                        |                        |                        |
|--|-----------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|----------------------|----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| ARI**<br>(years)   | <a href="#">5 min</a> | <a href="#">10 min</a> | <a href="#">15 min</a> | <a href="#">30 min</a> | <a href="#">60 min</a> | <a href="#">120 min</a> | <a href="#">3 hr</a> | <a href="#">6 hr</a> | <a href="#">12 hr</a> | <a href="#">24 hr</a> | <a href="#">48 hr</a> | <a href="#">4 day</a> | <a href="#">7 day</a> | <a href="#">10 day</a> | <a href="#">20 day</a> | <a href="#">30 day</a> | <a href="#">45 day</a> | <a href="#">60 day</a> |

MAPS

39° 56' 00" N  
39° 67'  
35° 50' 00"  
39° 66'  
39° 65'  
39° 64'

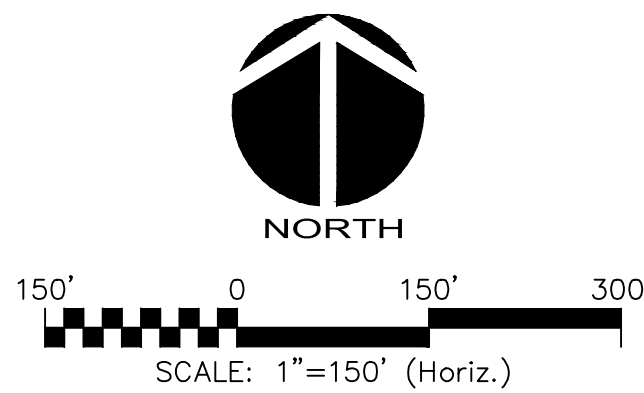
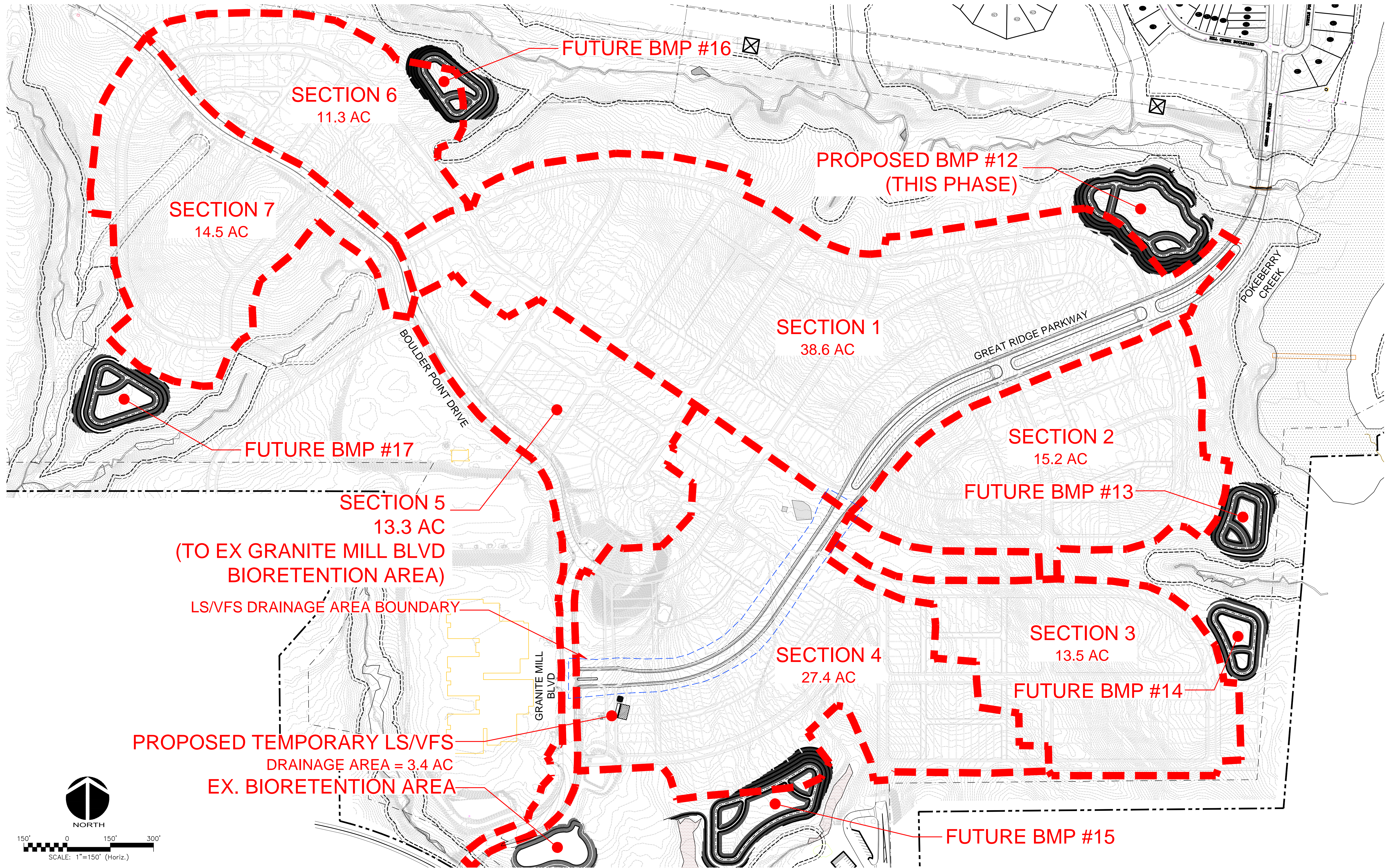


**Great Ridge  
Parkway Extension**



Great Ridge  
Parkway Extension





| REV. NO. | DESCRIPTION               | DATE       |
|----------|---------------------------|------------|
| 1        | SUBMITTAL TO DMO 401 UNIT | 2012.12.19 |
|          |                           |            |
|          |                           |            |
|          |                           |            |
|          |                           |            |
|          |                           |            |
|          |                           |            |
|          |                           |            |
|          |                           |            |

SEAL

SEAL

**MCKIM & CREED**  
 1730 Varsity Drive, Suite 500  
 Raleigh, North Carolina 27606  
 Phone: (919)233-8091, Fax: (919)233-8031  
 F-1222  
 www.mckimcreed.com

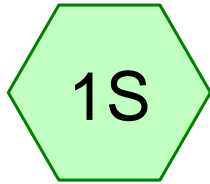
**BRIAR CHAPEL™**  
 by  
**Newland COMMUNITIES**

BRIAR CHAPEL  
 GREAT RIDGE PARKWAY EXTENSION  
 CHATHAM COUNTY, NORTH CAROLINA  
 BC SOUTH DRAINAGE AREA MAP

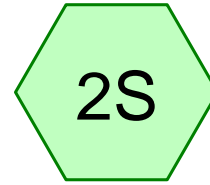
|                         |                       |                 |
|-------------------------|-----------------------|-----------------|
| DATE: DECEMBER 19, 2012 | SCALE                 | MAC FILE NUMBER |
| MCE PROJ. # 02735-0080  | HORIZONTAL: 1" = 150' | DA MAP          |
| DRAWN: GCA              | VERTICAL: N/A         | MAP 1           |
| DESIGNED: GCA           |                       |                 |
| CHECKED: CHS            |                       |                 |
| PROJ. MGR: CHS          |                       |                 |

|                         |             |
|-------------------------|-------------|
| STATUS: FOR PERMIT ONLY | REVISION: 1 |
|-------------------------|-------------|

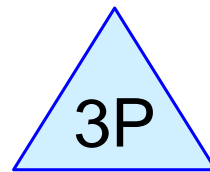
WET DETENTION POND  
#12 DESIGN



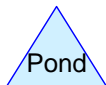
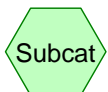
Pre-Development



Post-Development



BMP #11



**2012.12.05.Pond #12**

Type II 24-hr 1-inch Rainfall=1.00"

Prepared by {enter your company name here}

Printed 12/13/2012

HydroCAD® 10.00 s/n 04927 © 2011 HydroCAD Software Solutions LLC

Page 9

**Summary for Pond 3P: BMP #11**

Inflow Area = 39.152 ac, 66.12% Impervious, Inflow Depth = 0.32" for 1-inch event  
 Inflow = 15.42 cfs @ 12.08 hrs, Volume= 1.045 af  
 Outflow = 0.45 cfs @ 18.08 hrs, Volume= 0.742 af, Atten= 97%, Lag= 360.0 min  
 Primary = 0.45 cfs @ 18.08 hrs, Volume= 0.742 af  
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-40.00 hrs, dt= 0.05 hrs  
 Peak Elev= 414.98' @ 18.08 hrs Surf.Area= 64,092 sf Storage= 29,379 cf

Plug-Flow detention time= 662.2 min calculated for 0.742 af (71% of inflow)  
 Center-of-Mass det. time= 551.2 min ( 1,419.0 - 867.8 )

| Volume           | Invert            | Avail.Storage          | Storage Description  |
|------------------|-------------------|------------------------|--|
| #1               | 414.50'           | 332,222 cf             | <b>Custom Stage Data (Prismatic)</b> Listed below (Recalc) |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet)                                     |
| 414.50           | 59,103            | 0                      | 0  |
| 415.00           | 64,333            | 30,859                 | 30,859   |
| 416.00           | 67,546            | 65,940                 | 96,799   |
| 417.00           | 54,030            | 60,788                 | 157,587  |
| 418.00           | 56,787            | 55,409                 | 212,995  |
| 419.00           | 59,599            | 58,193                 | 271,188  |
| 420.00           | 62,468            | 61,034                 | 332,222  |

| Device | Routing   | Invert  | Outlet Devices  |
|--------|-----------|---------|---|
| #1     | Primary   | 411.00' | <b>30.0" Round Culvert</b><br>L= 55.0' RCP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 411.00' / 410.00' S= 0.0182 1/ S= 0.0182 1/ Cc= 0.900<br>n= 0.013, Flow Area= 4.91 sf |
| #2     | Device 1  | 414.50' | <b>6.0" Vert. Orifice/Grate</b> C= 0.600  |
| #3     | Device 1  | 416.00' | <b>30.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600  |
| #4     | Device 1  | 416.33' | <b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600<br>Limited to weir flow at low heads   |
| #5     | Secondary | 419.00' | <b>50.0' long x 16.0' breadth Broad-Crested Rectangular Weir</b><br>Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60<br>Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63          |

**Primary OutFlow** Max=0.45 cfs @ 18.08 hrs HW=414.98' (Free Discharge)

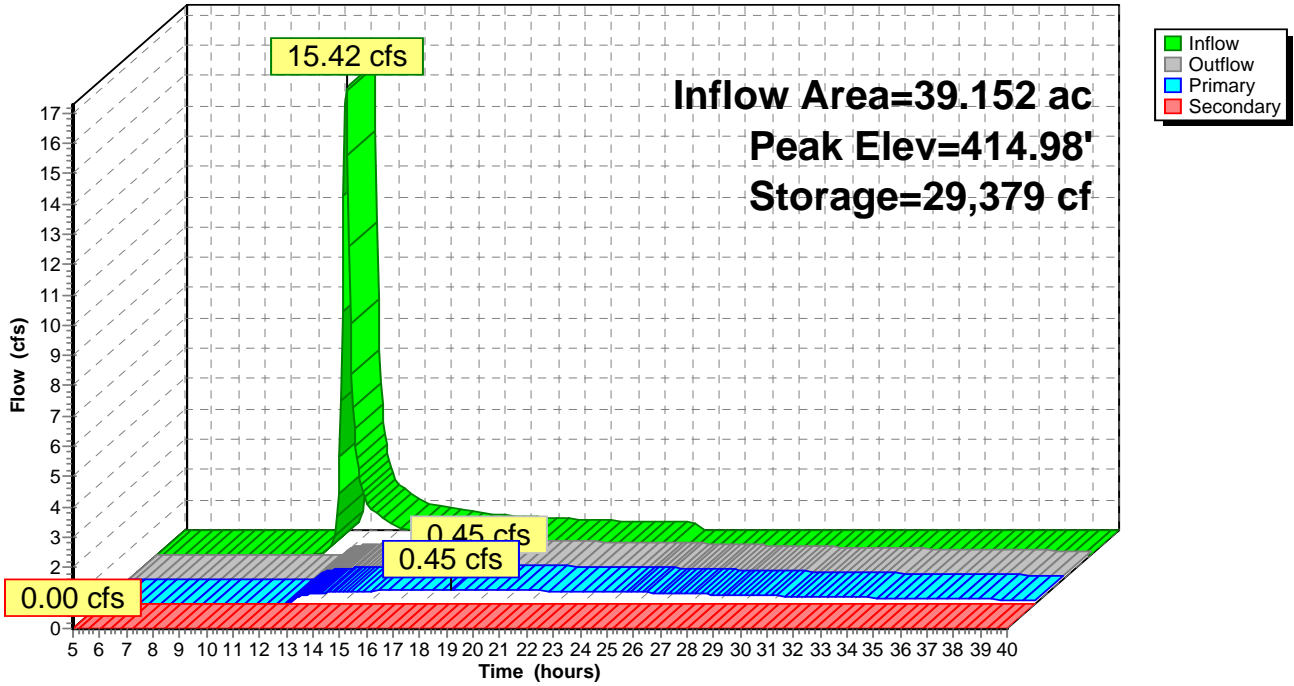
- 1=Culvert (Passes 0.45 cfs of 39.03 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 0.45 cfs @ 2.35 fps)
- 3=Orifice/Grate ( Controls 0.00 cfs)
- 4=Orifice/Grate ( Controls 0.00 cfs)

**Secondary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=414.50' (Free Discharge)

- 5=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

**Pond 3P: BMP #11**

Hydrograph



**2012.12.05.Pond #12**

Type II 24-hr 1-year Rainfall=2.96"

Prepared by {enter your company name here}

Printed 12/13/2012

HydroCAD® 10.00 s/n 04927 © 2011 HydroCAD Software Solutions LLC

Page 12

**Summary for Subcatchment 1S: Pre-Development**

Runoff = 19.71 cfs @ 12.28 hrs, Volume= 2.258 af, Depth= 0.69"

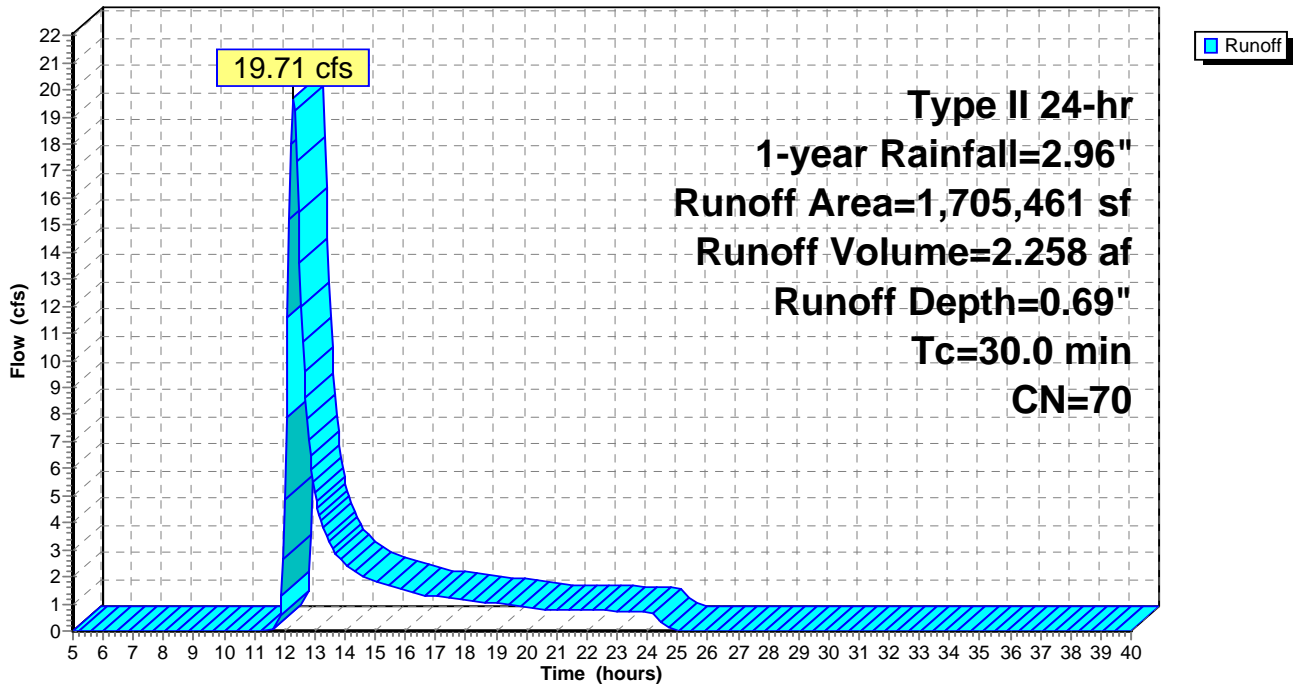
Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-40.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 1-year Rainfall=2.96"

| Area (sf) | CN | Description           |
|-----------|----|-----------------------|
| 1,705,461 | 70 | Woods, Good, HSG C    |
| 1,705,461 |    | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description   |
|----------|---------------|---------------|-------------------|----------------|---------------|
| 30.0     |               |               |                   |                | Direct Entry, |

**Subcatchment 1S: Pre-Development**

Hydrograph



**2012.12.05.Pond #12**

Type II 24-hr 1-year Rainfall=2.96"

Prepared by {enter your company name here}

Printed 12/13/2012

HydroCAD® 10.00 s/n 04927 © 2011 HydroCAD Software Solutions LLC

Page 14

**Summary for Pond 3P: BMP #11**

Inflow Area = 39.152 ac, 66.12% Impervious, Inflow Depth = 1.95" for 1-year event  
 Inflow = 96.85 cfs @ 12.07 hrs, Volume= 6.354 af  
 Outflow = 19.59 cfs @ 12.44 hrs, Volume= 5.149 af, Atten= 80%, Lag= 22.1 min  
 Primary = 19.59 cfs @ 12.44 hrs, Volume= 5.149 af  
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-40.00 hrs, dt= 0.05 hrs  
 Peak Elev= 416.77' @ 12.44 hrs Surf.Area= 57,174 sf Storage= 144,654 cf

Plug-Flow detention time= 428.6 min calculated for 5.149 af (81% of inflow)  
 Center-of-Mass det. time= 349.5 min ( 1,164.8 - 815.2 )

| Volume           | Invert            | Avail.Storage          | Storage Description  |
|------------------|-------------------|------------------------|--|
| #1               | 414.50'           | 332,222 cf             | <b>Custom Stage Data (Prismatic)</b> Listed below (Recalc) |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet)                                     |
| 414.50           | 59,103            | 0                      | 0  |
| 415.00           | 64,333            | 30,859                 | 30,859   |
| 416.00           | 67,546            | 65,940                 | 96,799   |
| 417.00           | 54,030            | 60,788                 | 157,587  |
| 418.00           | 56,787            | 55,409                 | 212,995  |
| 419.00           | 59,599            | 58,193                 | 271,188  |
| 420.00           | 62,468            | 61,034                 | 332,222  |

| Device | Routing   | Invert  | Outlet Devices   |
|--------|-----------|---------|--|
| #1     | Primary   | 411.00' | <b>30.0" Round Culvert</b><br>L= 55.0' RCP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 411.00' / 410.00' S= 0.0182 1/ S Cc= 0.900<br>n= 0.013, Flow Area= 4.91 sf   |
| #2     | Device 1  | 414.50' | <b>6.0" Vert. Orifice/Grate</b> C= 0.600   |
| #3     | Device 1  | 416.00' | <b>30.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600   |
| #4     | Device 1  | 416.33' | <b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600<br>Limited to weir flow at low heads  |
| #5     | Secondary | 419.00' | <b>50.0' long x 16.0' breadth Broad-Crested Rectangular Weir</b><br>Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60<br>Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63 |

**Primary OutFlow** Max=19.53 cfs @ 12.44 hrs HW=416.77' (Free Discharge)

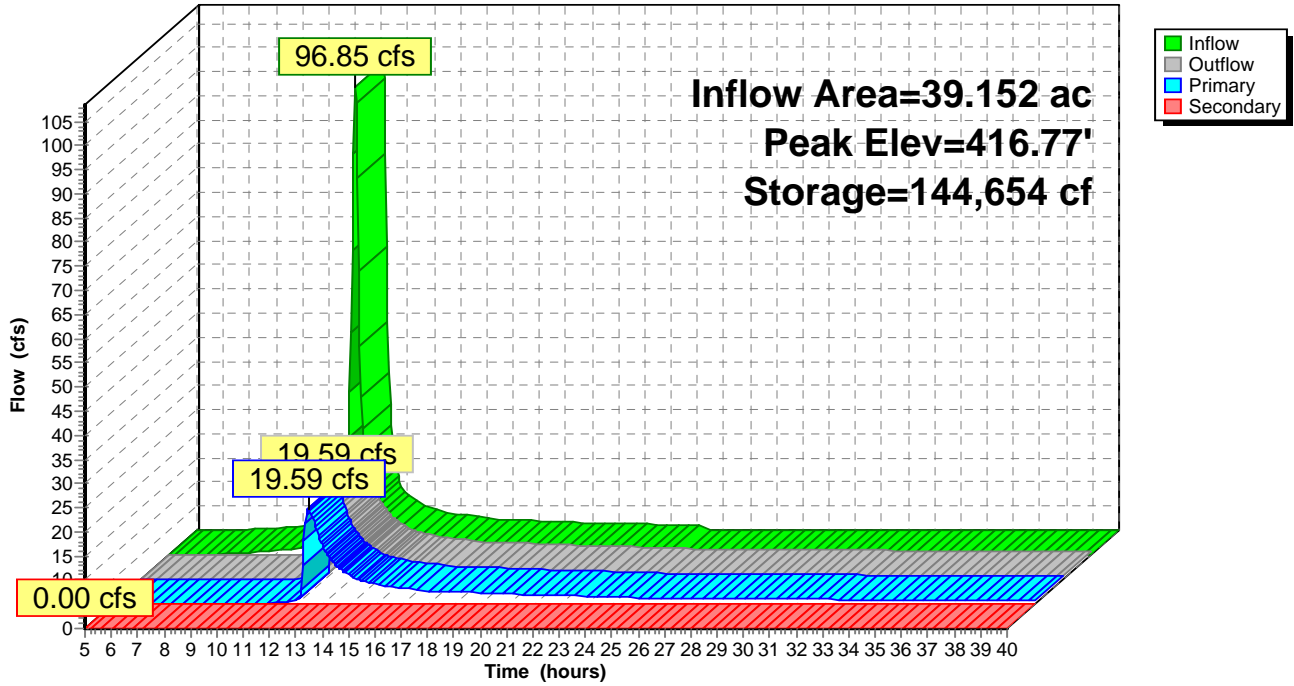
- 1=Culvert (Passes 19.53 cfs of 50.23 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 1.34 cfs @ 6.84 fps)
- 3=Orifice/Grate (Orifice Controls 3.10 cfs @ 3.72 fps)
- 4=Orifice/Grate (Weir Controls 15.09 cfs @ 2.16 fps)

**Secondary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=414.50' (Free Discharge)

- 5=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

### Pond 3P: BMP #11

Hydrograph





**2012.12.05.Pond #12**

Prepared by {enter your company name here}

HydroCAD® 10.00 s/n 04927 © 2011 HydroCAD Software Solutions LLC

Type II 24-hr 10-year Rainfall=5.17"

Printed 12/13/2012

Page 17

**Summary for Subcatchment 1S: Pre-Development**

Runoff = 71.57 cfs @ 12.26 hrs, Volume= 7.058 af, Depth= 2.16"

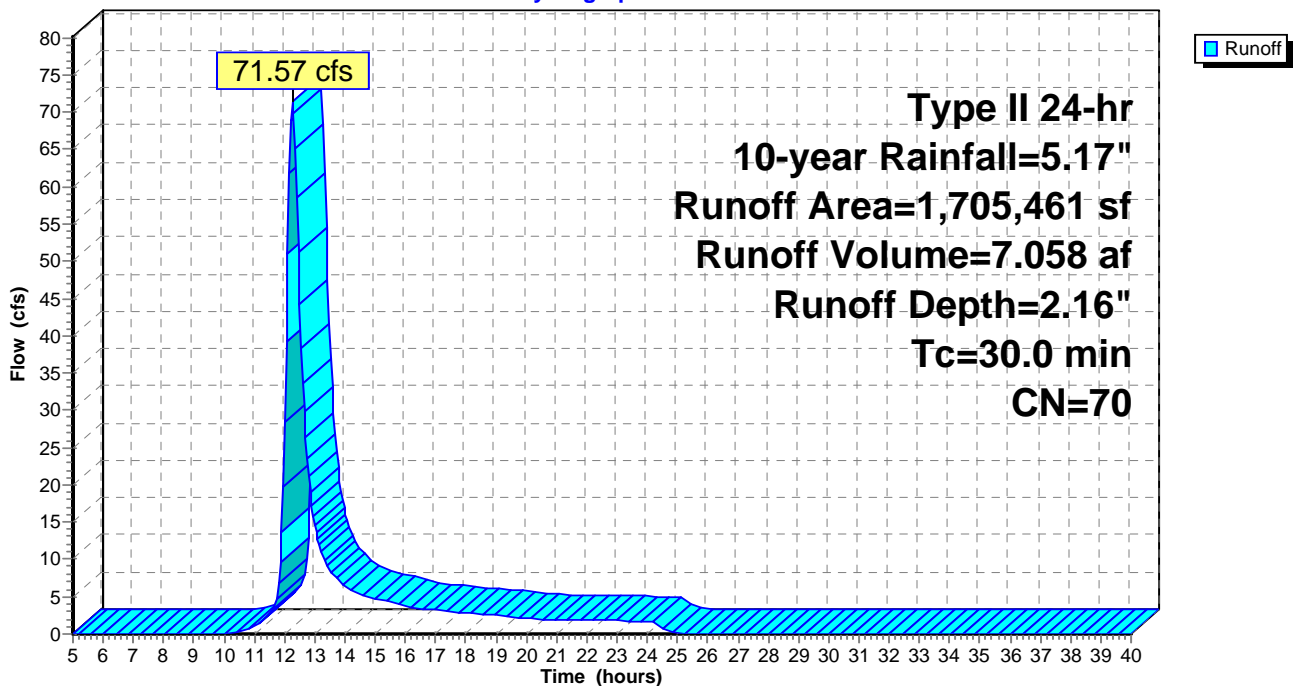
Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-40.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-year Rainfall=5.17"

| Area (sf) | CN | Description           |
|-----------|----|-----------------------|
| 1,705,461 | 70 | Woods, Good, HSG C    |
| 1,705,461 |    | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description   |
|----------|---------------|---------------|-------------------|----------------|---------------|
| 30.0     |               |               |                   |                | Direct Entry, |

**Subcatchment 1S: Pre-Development**

Hydrograph



**2012.12.05.Pond #12**

Type II 24-hr 10-year Rainfall=5.17"

Prepared by {enter your company name here}

Printed 12/13/2012

HydroCAD® 10.00 s/n 04927 © 2011 HydroCAD Software Solutions LLC

Page 19

**Summary for Pond 3P: BMP #11**

[82] Warning: Early inflow requires earlier time span

Inflow Area = 39.152 ac, 66.12% Impervious, Inflow Depth > 4.03" for 10-year event  
 Inflow = 194.70 cfs @ 12.06 hrs, Volume= 13.164 af  
 Outflow = 60.36 cfs @ 12.32 hrs, Volume= 11.867 af, Atten= 69%, Lag= 15.2 min  
 Primary = 60.36 cfs @ 12.32 hrs, Volume= 11.867 af  
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-40.00 hrs, dt= 0.05 hrs  
 Peak Elev= 418.77' @ 12.32 hrs Surf.Area= 58,957 sf Storage= 257,653 cf

Plug-Flow detention time= 234.1 min calculated for 11.866 af (90% of inflow)  
 Center-of-Mass det. time= 183.4 min ( 978.9 - 795.4 )

| Volume           | Invert            | Avail.Storage          | Storage Description  |
|------------------|-------------------|------------------------|--|
| #1               | 414.50'           | 332,222 cf             | <b>Custom Stage Data (Prismatic)</b> Listed below (Recalc) |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet)                                     |
| 414.50           | 59,103            | 0                      | 0  |
| 415.00           | 64,333            | 30,859                 | 30,859   |
| 416.00           | 67,546            | 65,940                 | 96,799   |
| 417.00           | 54,030            | 60,788                 | 157,587  |
| 418.00           | 56,787            | 55,409                 | 212,995  |
| 419.00           | 59,599            | 58,193                 | 271,188  |
| 420.00           | 62,468            | 61,034                 | 332,222  |

| Device | Routing   | Invert  | Outlet Devices  |
|--------|-----------|---------|---|
| #1     | Primary   | 411.00' | <b>30.0" Round Culvert</b><br>L= 55.0' RCP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 411.00' / 410.00' S= 0.0182 1/ S= 0.0182 1/ Cc= 0.900<br>n= 0.013, Flow Area= 4.91 sf |
| #2     | Device 1  | 414.50' | <b>6.0" Vert. Orifice/Grate</b> C= 0.600  |
| #3     | Device 1  | 416.00' | <b>30.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600  |
| #4     | Device 1  | 416.33' | <b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600<br>Limited to weir flow at low heads   |
| #5     | Secondary | 419.00' | <b>50.0' long x 16.0' breadth Broad-Crested Rectangular Weir</b><br>Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60<br>Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63          |

**Primary OutFlow** Max=60.33 cfs @ 12.32 hrs HW=418.77' (Free Discharge)

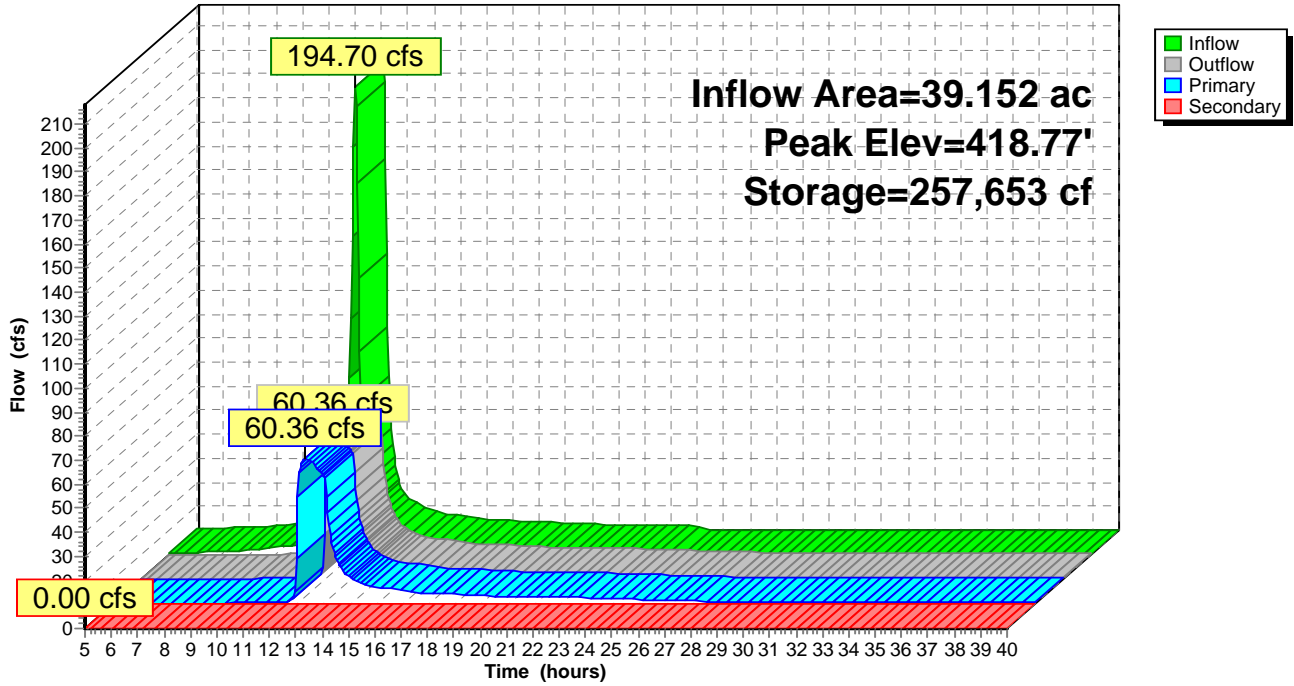
- 1=Culvert (Inlet Controls 60.33 cfs @ 12.29 fps)
- 2=Orifice/Grate (Passes < 1.89 cfs potential flow)
- 3=Orifice/Grate (Passes < 6.47 cfs potential flow)
- 4=Orifice/Grate (Passes < 120.24 cfs potential flow)

**Secondary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=414.50' (Free Discharge)

- 5=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

### Pond 3P: BMP #11

Hydrograph



**2012.12.05.Pond #12**

Type II 24-hr 100-year Rainfall=7.62"

Prepared by {enter your company name here}

Printed 12/13/2012

HydroCAD® 10.00 s/n 04927 © 2011 HydroCAD Software Solutions LLC

Page 22

**Summary for Subcatchment 1S: Pre-Development**

Runoff = 140.11 cfs @ 12.25 hrs, Volume= 13.506 af, Depth= 4.14"

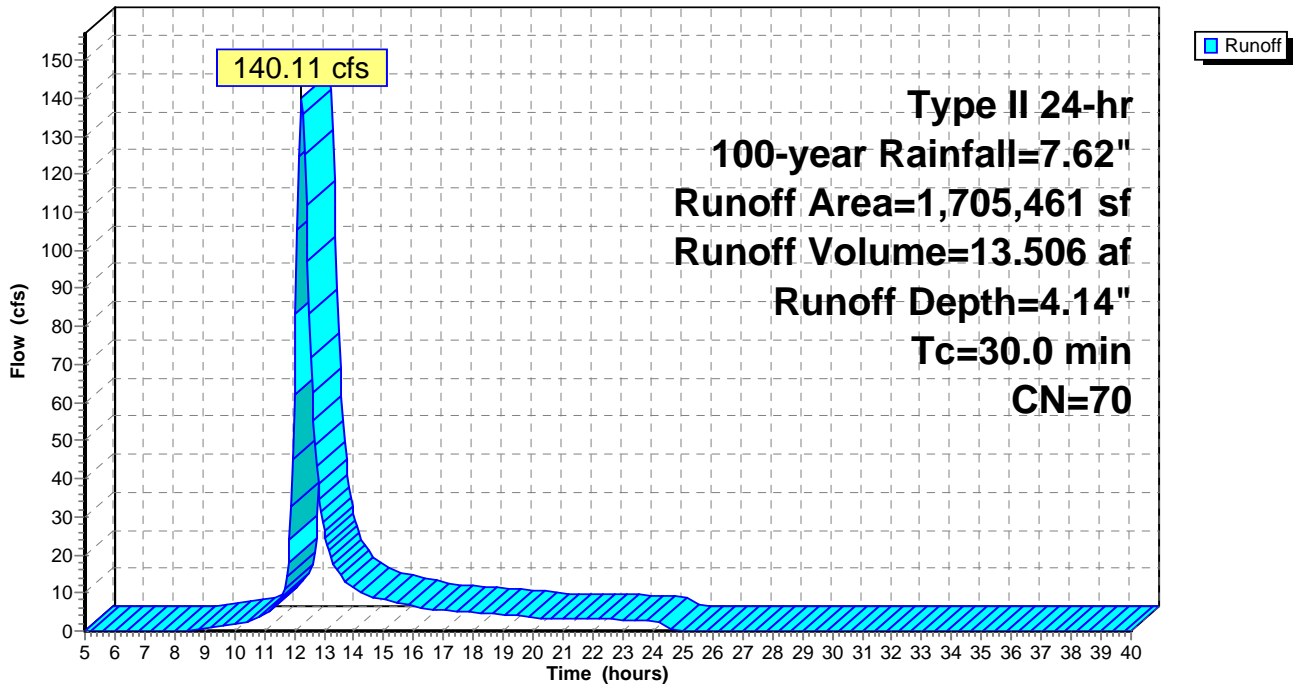
Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-40.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-year Rainfall=7.62"

| Area (sf) | CN | Description           |
|-----------|----|-----------------------|
| 1,705,461 | 70 | Woods, Good, HSG C    |
| 1,705,461 |    | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description   |
|----------|---------------|---------------|-------------------|----------------|---------------|
| 30.0     |               |               |                   |                | Direct Entry, |

**Subcatchment 1S: Pre-Development**

Hydrograph



**2012.12.05.Pond #12**

Type II 24-hr 100-year Rainfall=7.62"

Prepared by {enter your company name here}

Printed 12/13/2012

HydroCAD® 10.00 s/n 04927 © 2011 HydroCAD Software Solutions LLC

Page 24

**Summary for Pond 3P: BMP #11**

[82] Warning: Early inflow requires earlier time span

[93] Warning: Storage range exceeded by 0.05'

Inflow Area = 39.152 ac, 66.12% Impervious, Inflow Depth > 6.39" for 100-year event  
 Inflow = 302.03 cfs @ 12.06 hrs, Volume= 20.859 af  
 Outflow = 207.90 cfs @ 12.19 hrs, Volume= 19.529 af, Atten= 31%, Lag= 7.7 min  
 Primary = 66.02 cfs @ 12.19 hrs, Volume= 16.593 af  
 Secondary = 141.88 cfs @ 12.19 hrs, Volume= 2.936 af

Routing by Stor-Ind method, Time Span= 5.00-40.00 hrs, dt= 0.05 hrs  
 Peak Elev= 420.05' @ 12.19 hrs Surf.Area= 62,468 sf Storage= 332,222 cf

Plug-Flow detention time= 167.1 min calculated for 19.526 af (94% of inflow)  
 Center-of-Mass det. time= 130.9 min ( 916.3 - 785.4 )

| Volume | Invert  | Avail.Storage | Storage Description  |
|--------|---------|---------------|--|
| #1     | 414.50' | 332,222 cf    | <b>Custom Stage Data (Prismatic)</b> Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|------------------|-------------------|------------------------|------------------------|
| 414.50           | 59,103            | 0                      | 0                      |
| 415.00           | 64,333            | 30,859                 | 30,859                 |
| 416.00           | 67,546            | 65,940                 | 96,799                 |
| 417.00           | 54,030            | 60,788                 | 157,587                |
| 418.00           | 56,787            | 55,409                 | 212,995                |
| 419.00           | 59,599            | 58,193                 | 271,188                |
| 420.00           | 62,468            | 61,034                 | 332,222                |

| Device | Routing   | Invert  | Outlet Devices   |
|--------|-----------|---------|--|
| #1     | Primary   | 411.00' | <b>30.0" Round Culvert</b><br>L= 55.0' RCP, square edge headwall, Ke= 0.500<br>Inlet / Outlet Invert= 411.00' / 410.00' S= 0.0182 '/ Cc= 0.900<br>n= 0.013, Flow Area= 4.91 sf     |
| #2     | Device 1  | 414.50' | <b>6.0" Vert. Orifice/Grate</b> C= 0.600   |
| #3     | Device 1  | 416.00' | <b>30.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600   |
| #4     | Device 1  | 416.33' | <b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600<br>Limited to weir flow at low heads  |
| #5     | Secondary | 419.00' | <b>50.0' long x 16.0' breadth Broad-Crested Rectangular Weir</b><br>Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60<br>Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63 |

**Primary OutFlow** Max=65.94 cfs @ 12.19 hrs HW=420.03' (Free Discharge)

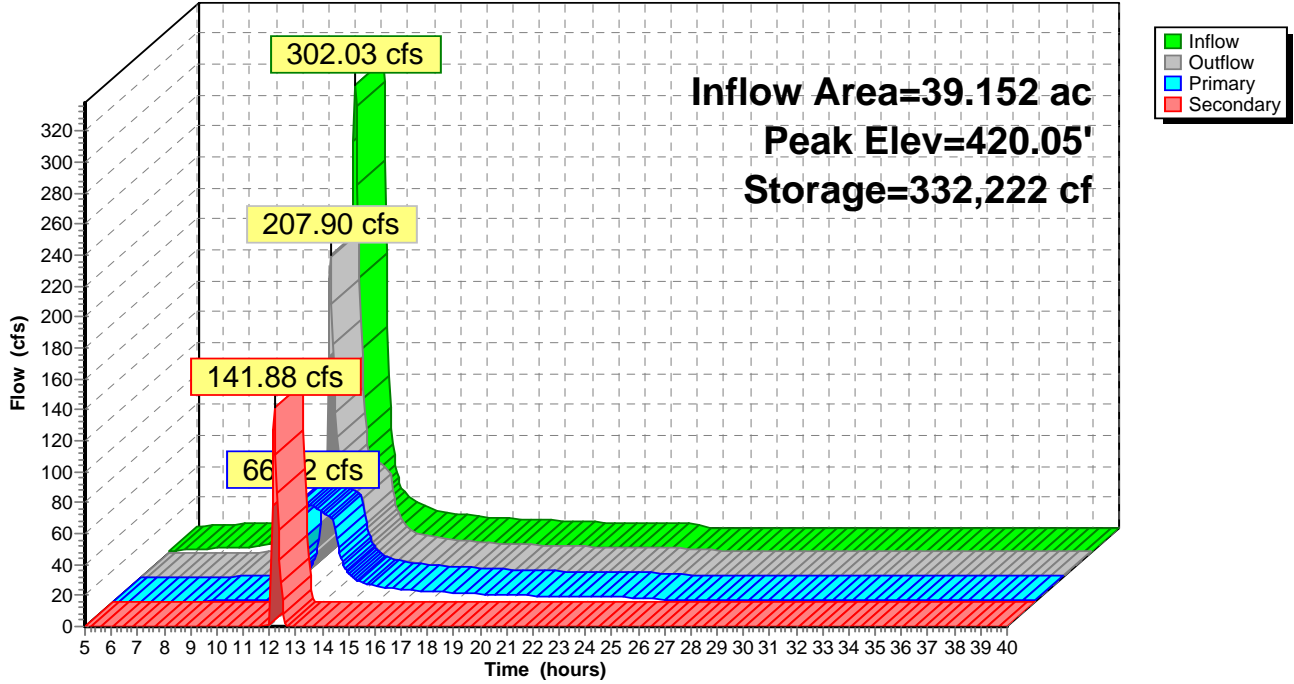
- ↑ 1=Culvert (Inlet Controls 65.94 cfs @ 13.43 fps)
- ↑ 2=Orifice/Grate (Passes < 2.17 cfs potential flow)
- ↑ 3=Orifice/Grate (Passes < 7.89 cfs potential flow)
- ↑ 4=Orifice/Grate (Passes < 148.27 cfs potential flow)

**Secondary OutFlow** Max=138.46 cfs @ 12.19 hrs HW=420.03' (Free Discharge)

- ↑ 5=Broad-Crested Rectangular Weir (Weir Controls 138.46 cfs @ 2.68 fps)

**Pond 3P: BMP #11**

Hydrograph



**WATER QUALITY POND #12 CALCULATIONS**

**Project Name**

Briar Chapel - Great Ridge Parkway Extension

**Project Number**

02735-0080

**Date**

December 14, 2012

3rd revision \_\_\_\_\_  
2nd revision \_\_\_\_\_  
1st revision \_\_\_\_\_

## Water Quality Pond Drainage Area Data

Project Briar Chapel - Great Ridge Parkway Extension

Project No. 02735-0080

Date December 14, 2012

Total site area 1,705,452 square feet = 39.15 acres

|                             | Drainage area to pond |               |             | Other Drainage Area |               |
|-----------------------------|-----------------------|---------------|-------------|---------------------|---------------|
|                             | Existing [sf]         | Proposed [sf] | Change [sf] | Existing [sf]       | Proposed [sf] |
| Impervious areas            |                       |               |             |                     |               |
| On-site buildings (BUA)     | 0                     | 630,800       | 630,800     | 0                   | 0             |
| On-site streets             | 0                     | 297,243       | 297,243     | 0                   | 0             |
| On-site alleys              | 0                     | 55,676        | 55,676      | 0                   | 0             |
| On-site sidewalks           | 0                     | 70,291        | 70,291      | 0                   | 0             |
| On-site future (open space) | 0                     | 10,000        | 10,000      | 0                   | 0             |
| Off-site streets            | 0                     | 0             | 0           | 0                   | 0             |
| 5% Contingency              | 0                     | 53,201        | 53,201      | 0                   | 0             |
| Total Impervious            | 0                     | 1,117,211     | 1,117,211   | 0                   | 0             |

|                               | Drainage area to pond |               |             | Other Drainage Area |               |
|-------------------------------|-----------------------|---------------|-------------|---------------------|---------------|
|                               | Existing [sf]         | Proposed [sf] | Change [sf] | Existing [sf]       | Proposed [sf] |
| Non-impervious areas          |                       |               |             |                     |               |
| On-site grass/landscape       | 0                     | 577,741       | 577,741     | 0                   | 0             |
| On-site woods                 | 1,705,452             | 0             | -1,705,452  | 0                   | 0             |
| Other undeveloped             | 0                     | 0             | 0           | 0                   | 0             |
| Total off-site non-impervious | 0                     | 0             | 0           | 0                   | 0             |
| Total non-impervious          | 1,705,452             | 577,741       | -1,127,711  | 0                   | 0             |

|                     |           |           |      |           |           |
|---------------------|-----------|-----------|------|-----------|-----------|
| Total Drainage Area | 1,705,452 | 1,705,452 | 0    | 3,167,850 | 3,167,850 |
| Percent Impervious  | 0.0       | 65.5      | 65.5 | 0.0       | 0.0       |

Notes:



## Water Quality Pond Surface Area Calculations

Project Briar Chapel - Great Ridge Parkway Extension  
Project No. 02735-0080

Date December 14, 2012

Total on-site drainage area to pond 1,705,452 square feet  
Total impervious area in drainage area 1,117,211 square feet

Average water depth of basin at normal pool 3.5 feet

Location of site Chatham County  
Site region Piedmont

% Impervious cover 65.5 percent

If the site is in a coastal area, will a vegetative filter be used? n/a

### Surface Area/Drainage Area Ratios:

For a site in the Piedmont (85%) 2.4 percent  
For a site in the Piedmont (90%) 3.4 percent  
For a site in a Coastal County w/ Vegetative Filter 4.9 percent  
For a site in a Coastal County w/out Vegetative Filter 6.6 percent

### Required surface area of pond:

For a site in the Piedmont (85%) 41,770.0 square feet  
For a site in the Piedmont (90%) 58,420.0 square feet  
For a site in a Coastal County w/ Vegetative Filter 83,030.0 square feet  
For a site in a Coastal County w/out Vegetative Filter 113,340.0 square feet

Notes:

## Water Quality Pond Stormwater Runoff Volume Calculations

Project Briar Chapel - Great Ridge Parkway Exten  
Project No. 02735-0080

Date December 14, 2012

Drainage area 1,705,452 square feet  
Impervious area 1,117,211 square feet  
Rainfall depth 1.00 inches

Percent Impervious 65.5 percent

$R(v) = 0.05 + 0.009 * (\text{Percent impervious})$

Runoff coefficient - R(v) 0.64 in/in

Runoff volume = (Design rainfall) \* (R(v)) \* (Drainage area)

Runoff volume 90,896.8 cubic feet

Notes:

**Water Quality Pond Volume Calculations  
Stage-Storage Data for Pond - Temporary Pool**

Project Briar Chapel - Great Ridge Parkway Extension  
 Project No. 02735-0080

Date December 14, 2012

| Contour ID | Stage | Area [sq. ft.] | Area [acres] | Incremental Area [sq. ft.] | Incremental Area [acres] | Incremental volume [cu. ft] | Incremental volume [acre-ft] | Cumulative volume [cu. ft] | Cumulative volume [acre-ft] |
|------------|-------|----------------|--------------|----------------------------|--------------------------|-----------------------------|------------------------------|----------------------------|-----------------------------|
| 414.5      | 0     | 59,103.0       | 1.357        | 59,103.0                   | 1.4                      | 0.0                         | 0.0                          | 0.0                        | 0.0                         |
| 415        | 0.5   | 64,333.0       | 1.477        | 5,230.0                    | 0.1                      | 30,859.0                    | 0.7                          | 30,859.0                   | 0.7                         |
| 416        | 1.5   | 67,546.0       | 1.551        | 3,213.0                    | 0.1                      | 65,939.5                    | 1.5                          | 96,798.5                   | 2.2                         |
| 417        | 2.5   | 70,785.0       | 1.625        | 3,239.0                    | 0.1                      | 69,165.5                    | 1.6                          | 165,964.0                  | 3.1                         |
| 418        | 3.5   | 74,142.0       | 1.702        | 3,357.0                    | 0.1                      | 72,463.5                    | 1.7                          | 238,427.5                  | 3.3                         |
| 419        | 4.5   | 77,525.0       | 1.780        | 3,383.0                    | 0.1                      | 75,833.5                    | 1.7                          | 314,261.0                  | 3.4                         |
| 420        | 5.5   | 80,965.0       | 1.859        | 3,440.0                    | 0.1                      | 79,245.0                    | 1.8                          | 393,506.0                  | 3.6                         |
| 421        | 6.5   | 84,461.0       | 1.939        | 3,496.0                    | 0.1                      | 82,713.0                    | 1.9                          | 476,219.0                  | 3.7                         |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |

**Water Quality Pond Volume Calculations**  
**Stage-Storage Data for Pond - Permanent Pool**

Project Briar Chapel - Great Ridge Parkway Extension  
 Project No. 02735-0080

Date December 14, 2012

| Contour ID | Stage | Area [sq. ft.] | Area [acres] | Incremental Area [sq. ft.] | Incremental Area [acres] | Incremental volume [cu. ft.] | Incremental volume [acre-ft] | Cumulative volume [cu. ft.] | Cumulative volume [acre-ft] |
|------------|-------|----------------|--------------|----------------------------|--------------------------|------------------------------|------------------------------|-----------------------------|-----------------------------|
| 410        | 0     | 35,993.0       | 0.826        | 35,993.0                   | 0.8                      | 0.0                          | 0.0                          | 0.0                         | 0.0                         |
| 411        | 1     | 39,840.0       | 0.915        | 3,847.0                    | 0.1                      | 37,916.5                     | 0.9                          | 37,916.5                    | 0.9                         |
| 412        | 2     | 43,903.0       | 1.008        | 4,063.0                    | 0.1                      | 41,871.5                     | 1.0                          | 79,788.0                    | 1.8                         |
| 413        | 3     | 48,095.0       | 1.104        | 4,192.0                    | 0.1                      | 45,999.0                     | 1.1                          | 125,787.0                   | 2.0                         |
| 414        | 4     | 52,458.0       | 1.204        | 4,363.0                    | 0.1                      | 50,276.5                     | 1.2                          | 176,063.5                   | 2.2                         |
| 414.5      | 4.5   | 59,103.0       | 1.357        | 6,645.0                    | 0.2                      | 27,890.3                     | 0.6                          | 203,953.8                   | 1.8                         |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |
|            |       |                |              |                            |                          |                              |                              |                             |                             |

**Water Quality Pond Volume Calculations  
Stage-Storage Data for Pond - Forebays**

Project Briar Chapel - Great Ridge Parkway Extension

Project No. 02735-0080

Date December 14, 2012

| Contour ID | Stage | Area [sq. ft.] | Area [acres] | Incremental Area [sq. ft.] | Incremental Area [acres] | Incremental volume [cu. ft] | Incremental volume [acre-ft] | Cumulative volume [cu. ft] | Cumulative volume [acre-ft] |
|------------|-------|----------------|--------------|----------------------------|--------------------------|-----------------------------|------------------------------|----------------------------|-----------------------------|
| 410        | 0     | 5,746.0        | 0.132        | 5,746.0                    | 0.1                      | 0.0                         | 0.0                          | 0.0                        | 0.0                         |
| 411        | 1     | 7,201.0        | 0.165        | 1,455.0                    | 0.0                      | 6,473.5                     | 0.1                          | 6,473.5                    | 0.1                         |
| 412        | 2     | 8,787.0        | 0.202        | 1,586.0                    | 0.0                      | 7,994.0                     | 0.2                          | 14,467.5                   | 0.3                         |
| 413        | 3     | 10,463.0       | 0.240        | 1,676.0                    | 0.0                      | 9,625.0                     | 0.2                          | 24,092.5                   | 0.4                         |
| 414        | 4     | 12,252.0       | 0.281        | 1,789.0                    | 0.0                      | 11,357.5                    | 0.3                          | 35,450.0                   | 0.5                         |
| 414.5      | 4.5   | 14,979.0       | 0.344        | 2,727.0                    | 0.1                      | 6,807.8                     | 0.2                          | 42,257.8                   | 0.4                         |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |
|            |       |                |              |                            |                          |                             |                              |                            |                             |

## Water Quality Basin Dewatering Time Calculations

Project Briar Chapel - Great Ridge Parkway Extension  
Project No. 02735-0080

Date December 14, 2012

|  |               |               |
|--|---------------|---------------|
| Maximum surface area of basin                | <u>67,546</u> | square feet   |
| Maximum head of water above dewatering hole  | <u>1.50</u>   | feet          |
| Orifice coefficient                          | <u>0.60</u>   |               |
| Diameter of each hole                        | <u>6.0</u>    | inches        |
| Number of holes                              | <u>1</u>      |               |
| Cross sectional area of each hole =          | <u>0.196</u>  | square feet   |
| Cross sectional area of each hole =          | <u>28.3</u>   | square inches |
| Cross sectional area of dewatering hole(s) = | <u>0.196</u>  | square feet   |
| Cross sectional area of dewatering hole(s) = | <u>28.3</u>   | square inches |
| Dewatering time for basin =                  | <u>48.6</u>   | hours         |
| Dewatering time for basin =                  | <u>2.03</u>   | days          |

Notes:

## Water Quality Pond Summary Information

Project Briar Chapel - Great Ridge Parkway  
Project No. 02735-0080

Date December 14, 2012

Drainage area to pond 1,705,452 square feet = 39.15 acres  
Impervious area in drainage area 1,117,211 square feet = 25.65 acres

Bottom of pond elevation 410.00 feet  
Normal pool elevation 414.50 feet  
Pond volume at normal pool 203,954 cubic feet

Required volume for design rainfall 90,897 cubic feet  
Required surface area for pond 58,420 square feet

Volume provided for storage of design rainfall = 96,799 cubic feet at elevation 416

Surface area provided at normal pool 59,103 square feet

**OUTLET PROTECTION  
DESIGN**

DATE: 12/05/2012

DESIGNED BY:  
GCA

PROJECT NAME: Briar Chapel - GRP Extension  
PROJECT LOCATION: Chatham County, NC

PROJECT NO:  
02735-0080

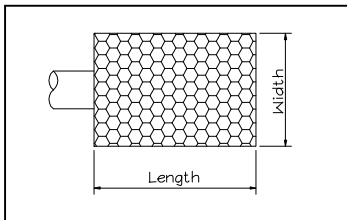
CHECKED BY  
GML

**Storm Outlet Structure**

Structure= **BMP #12 Out**  
Size= 30 in  
Q<sub>10</sub> = 60.36 cfs  
Q<sub>full</sub> = 55.24 cfs  
V<sub>full</sub> = 11.25 fps

Q<sub>10</sub>/Q<sub>full</sub> = 1.09  
V/V<sub>full</sub> = 1.112  
V = 12.5 fps

From Fig. 8.06.b.1:



Zone = **3**

D<sub>50</sub> = 10 in  
D<sub>MAX</sub> = 15 in  
Riprap Class = 1  
Apron Thickness = 24 in  
Apron Length = 20.0 ft  
Apron Width = 3 x Dia = 8.0 ft



|                               |                  |                  |
|-------------------------------|------------------|------------------|
| <b>ANTI-FLOATATION DESIGN</b> | DATE: 12/05/2012 | DESIGNED BY: GCA |
|-------------------------------|------------------|------------------|

|  |                           |                 |
|--|---------------------------|-----------------|
| PROJECT NAME: Briar Chapel GRP Extension<br>PROJECT LOCATION: Chatham County, NC | PROJECT NO:<br>02735-0080 | CHECKED BY: GML |
|--|---------------------------|-----------------|

|                        |         |                         |                        |
|------------------------|---------|-------------------------|------------------------|
| Pond Name=             | BMP #9  |                         |                        |
| Riser Outer Width =    | 5 ft    | Riser Resisting Force = | 7,871 lb               |
| Riser Outer Length =   | 5 ft    | Base Resisting Force =  | 7,350 lb               |
| Riser Inner Width =    | 4 ft    | Total Resisting Force = | 15,221 lb              |
| Riser Inner Length =   | 4 ft    |                         |                        |
| Riser Height =         | 5.83 ft | Riser Buoyant Force =   | 9,095 lb               |
|                        |         | Base Buoyant Force =    | 3,058 lb               |
| Concrete Base Length = | 7 ft    | Total Buoyant Force =   | 12,152 lb              |
| Concrete Base Width =  | 7 ft    |                         |                        |
| Concrete Base Depth =  | 12 in   | Factor of Safety        | 1.25 Design Acceptable |

# LS/VFS DESIGN

## Pipe Flowing Full Using Manning's Equation

$$D(\text{in}) = 8$$

$$\text{Slope} = 0.078$$

$$\text{Manning's } n = 0.011$$

$$Q_{\text{full}} = 3.981797 > 3.02\dots \text{ Therefore acceptable for outlet pipe for LS/VFS}$$

$$V_{\text{full}} = 11.40701$$

## Conduit FlexTable: Combined Pipe/Node Report (GRP Storm CAD.for GRP riprap sizing.stc)

| Label | Start Node | Stop Node | Length<br>(Unified)<br>(ft) | Upstream<br>Inlet C | Upstream<br>Intensity<br>(in/h) | Upstream<br>Inlet Area<br>(acres) | Upstream<br>Structure<br>Flow (Total<br>Surface)<br>(ft <sup>3</sup> /s) | System CA<br>(acres) | System<br>Intensity<br>(in/h) | System Rational<br>Flow<br>(ft <sup>3</sup> /s) |
|-------|------------|-----------|-----------------------------|---------------------|---------------------------------|-----------------------------------|--|----------------------|-------------------------------|---|
| CO-52 | CI-68      | CI-51     | 48.0                        | 0.650               | 1.000                           | 0.520                             | 0.34   | 0.345                | 1.000                         | 0.35  |
| CO-47 | CI-63      | CI-58     | 33.0                        | 0.750               | 1.000                           | 0.130                             | 0.10   | 0.097                | 1.000                         | 0.10  |
| CO-45 | CI-61      | CI-60     | 32.0                        | 0.750               | 1.000                           | 0.150                             | 0.11   | 0.111                | 1.000                         | 0.11  |
| CO-44 | CI-59      | CI-60     | 87.0                        | 0.750               | 1.000                           | 0.120                             | 0.09   | 0.201                | 1.000                         | 0.20  |
| CO-46 | CI-62      | CI-59     | 34.0                        | 0.750               | 1.000                           | 0.100                             | 0.08   | 0.076                | 1.000                         | 0.08  |
| CO-43 | CI-58      | CI-59     | 99.0                        | 0.750               | 1.000                           | 0.190                             | 0.14   | 0.418                | 1.000                         | 0.42  |
| CO-42 | CI-57      | CI-58     | 111.0                       | 0.750               | 1.000                           | 0.170                             | 0.13   | 0.643                | 1.000                         | 0.65  |
| CO-48 | CI-64      | CI-57     | 32.0                        | 0.750               | 1.000                           | 0.150                             | 0.11   | 0.112                | 1.000                         | 0.11  |
| CO-41 | CI-56      | CI-57     | 129.0                       | 0.750               | 1.000                           | 0.150                             | 0.11   | 0.869                | 1.000                         | 0.88  |
| CO-49 | CI-65      | CI-56     | 32.0                        | 0.750               | 1.000                           | 0.230                             | 0.17   | 0.169                | 1.000                         | 0.17  |
| CO-40 | CI-55      | CI-56     | 120.0                       | 0.750               | 1.000                           | 0.290                             | 0.22   | 1.246                | 1.000                         | 1.26  |
| CO-50 | CI-66      | CI-55     | 33.0                        | 0.750               | 1.000                           | 0.220                             | 0.17   | 0.165                | 1.000                         | 0.17  |
| CO-39 | CI-54      | CI-55     | 120.0                       | 0.750               | 1.000                           | 0.250                             | 0.19   | 1.601                | 1.000                         | 1.61  |
| CO-51 | CI-67      | CI-54     | 33.0                        | 0.750               | 1.000                           | 0.220                             | 0.17   | 0.165                | 1.000                         | 0.17  |
| CO-38 | CI-53      | CI-54     | 120.0                       | 0.750               | 1.000                           | 0.270                             | 0.20   | 1.967                | 1.000                         | 1.98  |
| CO-37 | CI-52      | CI-53     | 32.0                        | 0.750               | 1.000                           | 0.250                             | 0.19   | 2.156                | 1.000                         | 2.17  |
| CO-36 | CI-52      | CI-51     | 123.0                       | 0.750               | 1.000                           | 0.220                             | 0.17   | 2.321                | 1.000                         | 2.34  |
| CO-35 | CI-51      | FES-50    | 41.0                        | 0.750               | 1.000                           | 0.430                             | 0.33   | 2.993                | 1.000                         | 3.02  |
| CO-15 | CI-35      | CI-34     | 106.0                       | 0.750               | 1.000                           | 0.080                             | 0.06   | 0.908                | 1.000                         | 0.91  |
| CO-14 | CI-34      | CI-33     | 105.0                       | 0.750               | 1.000                           | 0.150                             | 0.11   | 1.388                | 1.000                         | 1.40  |
| CO-13 | CI-33      | CI-32     | 108.0                       | 0.750               | 1.000                           | 0.260                             | 0.20   | 1.580                | 1.000                         | 1.59  |
| CO-12 | CI-32      | CI-31     | 133.0                       | 0.750               | 1.000                           | 0.300                             | 0.23   | 1.802                | 1.000                         | 1.82  |
| CO-11 | CI-31      | CI-30     | 130.0                       | 0.750               | 1.000                           | 0.260                             | 0.20   | 1.999                | 1.000                         | 2.02  |
| CO-10 | CI-30      | CI-29     | 94.0                        | 0.750               | 1.000                           | 0.360                             | 0.27   | 2.261                | 1.000                         | 2.28  |
| CO-9  | CI-29      | CI-28     | 166.0                       | 0.750               | 1.000                           | 0.160                             | 0.12   | 2.393                | 1.000                         | 2.41  |
| CO-8  | CI-28      | CI-27     | 125.0                       | 0.750               | 1.000                           | 0.270                             | 0.20   | 2.585                | 1.000                         | 2.61  |
| CO-7  | CI-27      | CI-26     | 126.0                       | 0.750               | 1.000                           | 0.260                             | 0.20   | 2.778                | 1.000                         | 2.80  |
| CO-6  | CI-26      | CI-25     | 125.0                       | 0.750               | 1.000                           | 0.290                             | 0.22   | 2.992                | 1.000                         | 3.02  |
| CO-5  | CI-25      | CI-24     | 131.0                       | 0.750               | 1.000                           | 0.220                             | 0.17   | 3.168                | 1.000                         | 3.19  |
| CO-4  | CI-24      | CI-23     | 119.0                       | 0.750               | 1.000                           | 0.190                             | 0.14   | 3.315                | 1.000                         | 3.34  |

Permit Number: \_\_\_\_\_  
(to be provided by DWQ)

Drainage Area Number: \_\_\_\_\_

## Wet Detention Basin Operation and Maintenance Agreement

I will keep a maintenance record on this BMP. This maintenance record will be kept in a log in a known set location. Any deficient BMP elements noted in the inspection will be corrected, repaired or replaced immediately. These deficiencies can affect the integrity of structures, safety of the public, and the removal efficiency of the BMP.

The wet detention basin system is defined as the wet detention basin, pretreatment including forebays and the vegetated filter if one is provided.

**This system (check one):**

does  does not incorporate a vegetated filter at the outlet.

**This system (check one):**

does  does not incorporate pretreatment other than a forebay.

Important maintenance procedures:

- Immediately after the wet detention basin is established, the plants on the vegetated shelf and perimeter of the basin should be watered twice weekly if needed, until the plants become established (commonly six weeks).
- No portion of the wet detention pond should be fertilized after the first initial fertilization that is required to establish the plants on the vegetated shelf.
- Stable groundcover should be maintained in the drainage area to reduce the sediment load to the wet detention basin.
- If the basin must be drained for an emergency or to perform maintenance, the flushing of sediment through the emergency drain should be minimized to the maximum extent practical.
- Once a year, a dam safety expert should inspect the embankment.

After the wet detention pond is established, it should be inspected **once a month and within 24 hours after every storm event greater than 1.0 inches (or 1.5 inches if in a Coastal County)**. Records of operation and maintenance should be kept in a known set location and must be available upon request.

Inspection activities shall be performed as follows. Any problems that are found shall be repaired immediately.

| BMP element:                             | Potential problem:                                     | How I will remediate the problem:   |
|--|--|---|
| The entire BMP                           | Trash/debris is present.                               | Remove the trash/debris.  |
| The perimeter of the wet detention basin | Areas of bare soil and/or erosive gullies have formed. | Regrade the soil if necessary to remove the gully, and then plant a ground cover and water until it is established. Provide lime and a one-time fertilizer application. |
|  | Vegetation is too short or too long.                   | Maintain vegetation at a height of approximately six inches.  |

Permit Number: \_\_\_\_\_  
 (to be provided by DWQ)

Drainage Area Number: \_\_\_\_\_

| <b>BMP element:</b>                    | <b>Potential problem:</b>  | <b>How I will remediate the problem:</b>  |
|--|--|---|
| <b>The inlet device: pipe or swale</b> | The pipe is clogged.   | Unclog the pipe. Dispose of the sediment off-site.  |
|  | The pipe is cracked or otherwise damaged.  | Replace the pipe.   |
|  | Erosion is occurring in the swale.   | Regrade the swale if necessary to smooth it over and provide erosion control devices such as reinforced turf matting or riprap to avoid future problems with erosion.   |
| <b>The forebay</b>                     | Sediment has accumulated to a depth greater than the original design depth for sediment storage. | Search for the source of the sediment and remedy the problem if possible. Remove the sediment and dispose of it in a location where it will not cause impacts to streams or the BMP.  |
|  | Erosion has occurred.  | Provide additional erosion protection such as reinforced turf matting or riprap if needed to prevent future erosion problems.   |
|  | Weeds are present.   | Remove the weeds, preferably by hand. If pesticide is used, wipe it on the plants rather than spraying.   |
| <b>The vegetated shelf</b>             | Best professional practices show that pruning is needed to maintain optimal plant health.        | Prune according to best professional practices  |
|  | Plants are dead, diseased or dying.  | Determine the source of the problem: soils, hydrology, disease, etc. Remedy the problem and replace plants. Provide a one-time fertilizer application to establish the ground cover if a soil test indicates it is necessary. |
|  | Weeds are present.   | Remove the weeds, preferably by hand. If pesticide is used, wipe it on the plants rather than spraying.   |
| <b>The main treatment area</b>         | Sediment has accumulated to a depth greater than the original design sediment storage depth.     | Search for the source of the sediment and remedy the problem if possible. Remove the sediment and dispose of it in a location where it will not cause impacts to streams or the BMP.  |
|  | Algal growth covers over 50% of the area.  | Consult a professional to remove and control the algal growth.  |
|  | Cattails, phragmites or other invasive plants cover 50% of the basin surface.                    | Remove the plants by wiping them with pesticide (do not spray).   |

Permit Number: \_\_\_\_\_  
 (to be provided by DWQ)

Drainage Area Number: \_\_\_\_\_

| BMP element:               | Potential problem:  | How I will remediate the problem:  |
|----------------------------|---|--|
| <b>The embankment</b>      | Shrubs have started to grow on the embankment.  | Remove shrubs immediately.   |
|                            | Evidence of muskrat or beaver activity is present.  | Use traps to remove muskrats and consult a professional to remove beavers.                                 |
|                            | A tree has started to grow on the embankment.   | Consult a dam safety specialist to remove the tree.  |
|                            | An annual inspection by an appropriate professional shows that the embankment needs repair. (if applicable) | Make all needed repairs.   |
| <b>The outlet device</b>   | Clogging has occurred.  | Clean out the outlet device. Dispose of the sediment off-site.   |
|                            | The outlet device is damaged  | Repair or replace the outlet device.   |
| <b>The receiving water</b> | Erosion or other signs of damage have occurred at the outlet.   | Contact the local NC Division of Water Quality Regional Office, or the 401 Oversight Unit at 919-733-1786. |

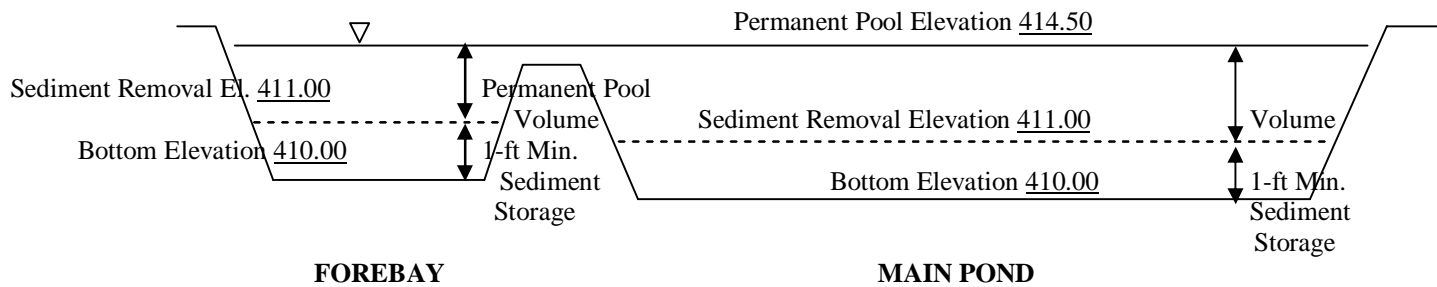
The measuring device used to determine the sediment elevation shall be such that it will give an accurate depth reading and not readily penetrate into accumulated sediments.

When the permanent pool depth reads 3.50 feet in the main pond, the sediment shall be removed.

When the permanent pool depth reads 3.50 feet in the forebay, the sediment shall be removed.

### BASIN DIAGRAM

(fill in the blanks)



Permit Number: \_\_\_\_\_  
(to be provided by DWQ)

I acknowledge and agree by my signature below that I am responsible for the performance of the maintenance procedures listed above. I agree to notify DWQ of any problems with the system or prior to any changes to the system or responsible party.

Project name: Briar Chapel - Great Ridge Parkway Extension

BMP drainage area number: 1 - Wet Detention Pond #12

Print name: Kevin Graham

Title: Vice President, Operations

Address: 16 Windy Knoll Circle, Chapel Hill, NC 27516

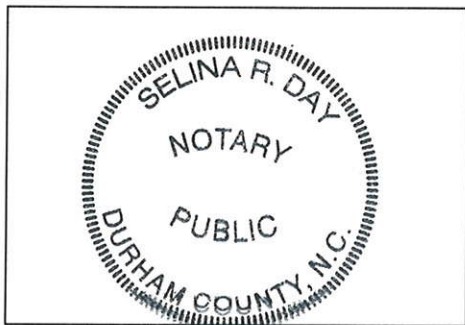
Phone: (919) 951-0709

Signature: *Kevin Graham*

Date: 12/13/12

Note: The legally responsible party should not be a homeowners association unless more than 50% of the lots have been sold and a resident of the subdivision has been named the president.

I, Selina R. Day, a Notary Public for the State of North Carolina, County of Durham, do hereby certify that Kevin Graham personally appeared before me this 13 day of December, 2012, and acknowledge the due execution of the forgoing wet detention basin maintenance requirements. Witness my hand and official seal,



SEAL

My commission expires August 30, 2014



Permit Number: \_\_\_\_\_  
(to be provided by DWQ)

Drainage Area Number: \_\_\_\_\_

## Filter Strip, Restored Riparian Buffer and Level Spreader Operation and Maintenance Agreement

I will keep a maintenance record on this BMP. This maintenance record will be kept in a log in a known set location. Any deficient BMP elements noted in the inspection will be corrected, repaired or replaced immediately. These deficiencies can affect the integrity of structures, safety of the public, and the removal efficiency of the BMP.

Important maintenance procedures:

- Immediately after the filter strip is established, any newly planted vegetation will be watered twice weekly if needed until the plants become established (commonly six weeks).
- Once a year, the filter strip will be reseeded to maintain a dense growth of vegetation
- Stable groundcover will be maintained in the drainage area to reduce the sediment load to the vegetation.
- Two to three times a year, grass filter strips will be mowed and the clippings harvested to promote the growth of thick vegetation with optimum pollutant removal efficiency. Turf grass should not be cut shorter than 3 to 5 inches and may be allowed to grow as tall as 12 inches depending on aesthetic requirements (NIPC, 1993). Forested filter strips do not require this type of maintenance.
- Once a year, the soil will be aerated if necessary.
- Once a year, soil pH will be tested and lime will be added if necessary.

After the filter strip is established, it will be inspected **quarterly and within 24 hours after every storm event greater than 1.0 inch (or 1.5 inches if in a Coastal County)**. Records of operation and maintenance will be kept in a known set location and will be available upon request.

Inspection activities shall be performed as follows. Any problems that are found shall be repaired immediately.

| BMP element:                             | Potential problem:                   | How I will remediate the problem:  |
|--|--------------------------------------|--|
| The entire filter strip system           | Trash/debris is present.             | Remove the trash/debris.   |
| The flow splitter device (if applicable) | The flow splitter device is clogged. | Unclog the conveyance and dispose of any sediment off-site.              |
|  | The flow splitter device is damaged. | Make any necessary repairs or replace if damage is too large for repair. |

| <b>BMP element:</b>                | <b>Potential problem:</b>  | <b>How I will remediate the problem:</b>  |
|------------------------------------|--|---|
| <b>The swale and the level lip</b> | The swale is clogged with sediment.  | Remove the sediment and dispose of it off-site.   |
|                                    | The level lip is cracked, settled, undercut, eroded or otherwise damaged.                    | Repair or replace lip.  |
|                                    | There is erosion around the end of the level spreader that shows stormwater has bypassed it. | Regrade the soil to create a berm that is higher than the level lip, and then plant a ground cover and water until it is established. Provide lime and a one-time fertilizer application. |
|                                    | Trees or shrubs have begun to grow on the swale or just downslope of the level lip.          | Remove them.  |
| <b>The bypass channel</b>          | Areas of bare soil and/or erosive gullies have formed.                                       | Regrade the soil if necessary to remove the gully, and then reestablish proper erosion control.   |
|                                    | Turf reinforcement is damaged or riprap is rolling downhill.                                 | Study the site to see if a larger bypass channel is needed (enlarge if necessary). After this, reestablish the erosion control material.  |
| <b>The filter strip</b>            | Grass is too short or too long (if applicable).  | Maintain grass at a height of approximately three to six inches.  |
|                                    | Areas of bare soil and/or erosive gullies have formed.                                       | Regrade the soil if necessary to remove the gully, and then plant a ground cover and water until it is established. Provide lime and a one-time fertilizer application.                   |
|                                    | Sediment is building up on the filter strip.   | Remove the sediment and restabilize the soil with vegetation if necessary. Provide lime and a one-time fertilizer application.  |
|                                    | Plants are desiccated.   | Provide additional irrigation and fertilizer as needed.   |
|                                    | Plants are dead, diseased or dying.  | Determine the source of the problem: soils, hydrology, disease, etc. Remedy the problem and replace plants. Provide a one-time fertilizer application.                                    |
|                                    | Nuisance vegetation is choking out desirable species.  | Remove vegetation by hand if possible. If pesticide is used, do not allow it to get into the receiving water.   |
| <b>The receiving water</b>         | Erosion or other signs of damage have occurred at the outlet.                                | Contact the NC Division of Water Quality local Regional Office, or the 401 Oversight Unit at 919-733-1786.  |

Permit Number: \_\_\_\_\_  
(to be provided by DWQ)

I acknowledge and agree by my signature below that I am responsible for the performance of the maintenance procedures listed above. I agree to notify DWQ of any problems with the system or prior to any changes to the system or responsible party.

Project name: Briar Chapel - Great Ridge Parkway Extension


BMP drainage area number: #2 - LS/VFS #1

Print name: Kevin Graham

Title: Vice President, Operations

Address: 16 Windy Knoll Circle, Chapel Hill, NC 27516

Phone: (919) 951-0709

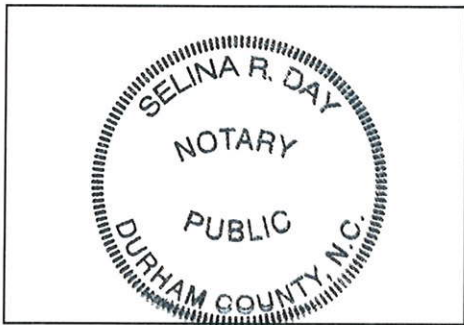
Signature: 

Date: 12/13/12

Note: The legally responsible party should not be a homeowners association unless more than 50% of the lots have been sold and a resident of the subdivision has been named the president.

I, Selina R. Day, a Notary Public for the State of North Carolina, County of Durham, do hereby certify that Kevin Graham personally appeared before me this 13 day of December, 2012, and acknowledge the due execution of the forgoing filter strip, riparian buffer, and/or level spreader maintenance requirements.

Witness my hand and official seal,



SEAL

My commission expires August 30, 2014



STORMWATER MANAGEMENT PERMIT APPLICATION FORM  
401 CERTIFICATION APPLICATION FORM  
**WET DETENTION BASIN SUPPLEMENT**

*This form must be filled out, printed and submitted.*

*The Required Items Checklist (Part III) must be printed, filled out and submitted along with all of the required information.*

**I. PROJECT INFORMATION**

|                      |  |
|----------------------|--|
| Project name         | Briar Chapel Development - Great Ridge Parkway Extension |
| Contact person       | Gareth Avant, PE   |
| Phone number         | 919.233.8091   |
| Date                 | 14-Dec-2012  |
| Drainage area number | 1 - Wet Pond #13   |

**II. DESIGN INFORMATION**

|  |           |  |
|--|-----------|--|
| Site Characteristics   |           |  |
| Drainage area  | 1,705,452 | ft <sup>2</sup>  |
| Impervious area, post-development                                      | 1,117,211 | ft <sup>2</sup>  |
| % impervious   | 65.51     | %  |
| Design rainfall depth  | 1.0       | in   |
| Storage Volume: Non-SA Waters  |           |  |
| Minimum volume required  | 90,897    | ft <sup>3</sup> OK   |
| Volume provided  | 96,799    | ft <sup>3</sup> OK, volume provided is equal to or in excess of volume required. |
| Storage Volume: SA Waters  |           |  |
| 1.5" runoff volume   |           | ft <sup>3</sup>  |
| Pre-development 1-yr, 24-hr runoff                                     |           | ft <sup>3</sup>  |
| Post-development 1-yr, 24-hr runoff                                    |           | ft <sup>3</sup>  |
| Minimum volume required  |           | ft <sup>3</sup>  |
| Volume provided  |           | ft <sup>3</sup>  |
| Peak Flow Calculations   |           |  |
| Is the pre/post control of the 1yr 24hr storm peak flow required?      | Y         | (Y or N)   |
| 1-yr, 24-hr rainfall depth   | 3.0       | in   |
| Rational C, pre-development  | 0.40      | (unitless)   |
| Rational C, post-development   | 0.72      | (unitless)   |
| Rainfall intensity: 1-yr, 24-hr storm                                  | 0.12      | in/hr Insufficient. Check intensity calculation.                                 |
| Pre-development 1-yr, 24-hr peak flow                                  | 19.71     | ft <sup>3</sup> /sec   |
| Post-development 1-yr, 24-hr peak flow                                 | 19.59     | ft <sup>3</sup> /sec   |
| Pre/Post 1-yr, 24-hr peak flow control                                 | -0.12     | ft <sup>3</sup> /sec   |
| Elevations   |           |  |
| Temporary pool elevation   | 416.00    | fmsl   |
| Permanent pool elevation   | 414.50    | fmsl   |
| SHWT elevation (approx. at the perm. pool elevation)                   |           | fmsl   |
| Top of 10ft vegetated shelf elevation                                  | 415.00    | fmsl   |
| Bottom of 10ft vegetated shelf elevation                               | 414.00    | fmsl   |
| Sediment cleanout, top elevation (bottom of pond)                      | 411.00    | fmsl   |
| Sediment cleanout, bottom elevation                                    | 410.00    | fmsl   |
| Sediment storage provided  | 1.00      | ft   |
| Is there additional volume stored above the state-required temp. pool? | N         | (Y or N)   |
| Elevation of the top of the additional volume                          |           | fmsl   |

**II. DESIGN INFORMATION**

## Surface Areas

|  |        |                 |    |
|--|--------|-----------------|----|
| Area, temporary pool   | 59,103 | ft <sup>2</sup> |    |
| Area REQUIRED, permanent pool  | 51,164 | ft <sup>2</sup> |    |
| SA/DA ratio  | 3.00   | (unitless)      |    |
| Area PROVIDED, permanent pool, $A_{perm\_pool}$                          | 59,103 | ft <sup>2</sup> | OK |
| Area, bottom of 10ft vegetated shelf, $A_{bot\_shelf}$                   | 52,458 | ft <sup>2</sup> |    |
| Area, sediment cleanout, top elevation (bottom of pond), $A_{bot\_pond}$ | 35,993 | ft <sup>2</sup> |    |

## Volumes

|  |         |                 |    |
|--|---------|-----------------|----|
| Volume, temporary pool                                     | 96,799  | ft <sup>3</sup> | OK |
| Volume, permanent pool, $V_{perm\_pool}$                   | 203,954 | ft <sup>3</sup> |    |
| Volume, forebay (sum of forebays if more than one forebay) | 42,258  | ft <sup>3</sup> |    |
| Forebay % of permanent pool volume                         | 20.7%   | %               | OK |

## SA/DA Table Data

|                                     |      |            |  |
|-------------------------------------|------|------------|--|
| Design TSS removal                  | 90   | %          |  |
| Coastal SA/DA Table Used?           | N    | (Y or N)   |  |
| Mountain/Piedmont SA/DA Table Used? | Y    | (Y or N)   |  |
| SA/DA ratio                         | 3.00 | (unitless) |  |

## Average depth (used in SA/DA table):

|  |         |                 |    |
|--|---------|-----------------|----|
| Calculation option 1 used? (See Figure 10-2b)                    | Y       | (Y or N)        |    |
| Volume, permanent pool, $V_{perm\_pool}$                         | 203,954 | ft <sup>3</sup> |    |
| Area provided, permanent pool, $A_{perm\_pool}$                  | 59,103  | ft <sup>2</sup> |    |
| Average depth calculated   | 3.45    | ft              | OK |
| Average depth used in SA/DA, $d_{av}$ , (Round to nearest 0.5ft) | 3.5     | ft              | OK |

Calculation option 2 used? (See Figure 10-2b)

|  |        |                 |  |
|--|--------|-----------------|--|
| Area provided, permanent pool, $A_{perm\_pool}$                          | 59,103 | ft <sup>2</sup> |  |
| Area, bottom of 10ft vegetated shelf, $A_{bot\_shelf}$                   | 52,458 | ft <sup>2</sup> |  |
| Area, sediment cleanout, top elevation (bottom of pond), $A_{bot\_pond}$ | 35,993 | ft <sup>2</sup> |  |

"Depth" (distance b/w bottom of 10ft shelf and top of sediment)

Average depth calculated

 Average depth used in SA/DA,  $d_{av}$ , (Round to nearest 0.5ft)

## Drawdown Calculations

|   |       |                      |                             |
|---|-------|----------------------|-----------------------------|
| Drawdown through orifice?   | Y     | (Y or N)             |                             |
| Diameter of orifice (if circular)                                 | 6.00  | in                   |                             |
| Area of orifice (if non-circular)                                 |       | in <sup>2</sup>      |                             |
| Coefficient of discharge ( $C_D$ )                                | 0.60  | (unitless)           |                             |
| Driving head ( $H_0$ )  | 0.50  | ft                   |                             |
| Drawdown through weir?  | N     | (Y or N)             |                             |
| Weir type   |       | (unitless)           |                             |
| Coefficient of discharge ( $C_w$ )                                |       | (unitless)           |                             |
| Length of weir (L)  |       | ft                   |                             |
| Driving head (H)  |       | ft                   |                             |
| Pre-development 1-yr, 24-hr peak flow                             | 19.71 | ft <sup>3</sup> /sec |                             |
| Post-development 1-yr, 24-hr peak flow                            | 19.59 | ft <sup>3</sup> /sec |                             |
| Storage volume discharge rate (through discharge orifice or weir) | 0.45  | ft <sup>3</sup> /sec |                             |
| Storage volume drawdown time                                      | 2.03  | days                 | OK, draws down in 2-5 days. |

## Additional Information

|  |                        |          |    |
|--|------------------------|----------|----|
| Vegetated side slopes                              | 3                      | :1       | OK |
| Vegetated shelf slope                              | 10                     | :1       | OK |
| Vegetated shelf width                              | 10.0                   | ft       | OK |
| Length of flowpath to width ratio                  | 3                      | :1       | OK |
| Length to width ratio                              | 1.5                    | :1       | OK |
| Trash rack for overflow & orifice?                 | Y                      | (Y or N) | OK |
| Freeboard provided                                 | 1.0                    | ft       | OK |
| Vegetated filter provided?                         | N                      | (Y or N) | OK |
| Recorded drainage easement provided?               | Y                      | (Y or N) | OK |
| Capures all runoff at ultimate build-out?          | Y                      | (Y or N) | OK |
| Drain mechanism for maintenance or emergencies is: | 8" DIP with gate valve |          |    |

**III. REQUIRED ITEMS CHECKLIST**

Please indicate the page or plan sheet numbers where the supporting documentation can be found. An incomplete submittal package will result in a request for additional information. This will delay final review and approval of the project. Initial in the space provided to indicate the following design requirements have been met. If the applicant has designated an agent, the agent may initial below. If a requirement has not been met, attach justification.

| Initials | Page/ Plan Sheet No. |  |
|----------|----------------------|--|
| GCA      | C3.3-C3.4            | 1. Plans (1" - 50' or larger) of the entire site showing: <ul style="list-style-type: none"> <li>- Design at ultimate build-out,</li> <li>- Off-site drainage (if applicable),</li> <li>- Delineated drainage basins (include Rational C coefficient per basin),</li> <li>- Basin dimensions,</li> <li>- Pretreatment system,</li> <li>- High flow bypass system,</li> <li>- Maintenance access,</li> <li>- Proposed drainage easement and public right of way (ROW),</li> <li>- Overflow device, and</li> <li>- Boundaries of drainage easement.</li> </ul> |
| GCA      | D4.1-D4.3            | 2. Partial plan (1" = 30' or larger) and details for the wet detention basin showing: <ul style="list-style-type: none"> <li>- Outlet structure with trash rack or similar,</li> <li>- Maintenance access,</li> <li>- Permanent pool dimensions,</li> <li>- Forebay and main pond with hardened emergency spillway,</li> <li>- Basin cross-section,</li> <li>- Vegetation specification for planting shelf, and</li> <li>- Filter strip.</li> </ul>  |
| GCA      | D4.1-D4.3            | 3. Section view of the wet detention basin (1" = 20' or larger) showing: <ul style="list-style-type: none"> <li>- Side slopes, 3:1 or lower,</li> <li>- Pretreatment and treatment areas, and</li> <li>- Inlet and outlet structures.</li> </ul>   |
| GCA      | N/A                  | 4. If the basin is used for sediment and erosion control during construction, clean out of the basin is specified on the plans prior to use as a wet detention basin.  |
| GCA      | Calc Booklet         | 5. A table of elevations, areas, incremental volumes & accumulated volumes for overall pond and for forebay, to verify volume provided.  |
| GCA      | C3.1                 | 6. A construction sequence that shows how the wet detention basin will be protected from sediment until the entire drainage area is stabilized.  |
| GCA      | Calc Booklet         | 7. The supporting calculations.  |
| GCA      | Included             | 8. A copy of the signed and notarized operation and maintenance (O&M) agreement.   |
| GCA      | Included             | 9. A copy of the deed restrictions (if required).  |
| _____    | N/A                  | 10. A soils report that is based upon an actual field investigation, soil borings, and infiltration tests. County soil maps are not an acceptable source of soils information.   |



STORMWATER MANAGEMENT PERMIT APPLICATION FORM  
401 CERTIFICATION APPLICATION FORM  
**LEVEL SPREADER - VEGETATED FILTER STRIP (LS-VFS) SUPPLEMENT**

*This form must be completely filled out, printed, initialed, and submitted.*

**I. PROJECT INFORMATION**

|                      |  |
|----------------------|--|
| Project name         | Briar Chapel Development - Great Ridge Parkway Extension |
| Contact name         | Gareth Avant   |
| Phone number         | 919.233.8091   |
| Date                 | December 14, 2012  |
| Drainage area number | #2   |

**II. DESIGN INFORMATION**

|  |   |
|--|---|
| The purpose of the LS-VFS                  | Pollutant removal: 40% TSS, 30% TN, 35% TP            |
| Stormwater enters LS-VFS from              | The drainage area                                     |
| Type of VFS                                | Engineered filter strip (graded & sodded, slope < 8%) |
| Explanation of any "Other" responses above |   |

**If Stormwater Enters the LS-VFS from the Drainage Area**

|   |                   |                 |
|---|-------------------|-----------------|
| Drainage area                                 | 147,452           | ft <sup>2</sup> |
| Impervious surface area                       | 62,438            | ft <sup>2</sup> |
| Percent impervious                            | 42.34             | %               |
| Rational C coefficient                        | 0.75              |                 |
| Peak flow from the 1 in/hr storm              | 2.54              | cfs             |
| Time of concentration                         | 5.00              | min             |
| Rainfall intensity, 10-yr storm               | 7.38              | in/hr           |
| Peak flow from the 10-yr storm                | 18.74             | cfs             |
| Design storm                                  | 1 inch/hour storm |                 |
| Maximum amount of flow directed to the LS-VFS | 3.02              | cfs             |
| Is a flow bypass system going to be used?     | Y                 | (Y or N)        |
| Explanation of any "Other" responses above    |                   |                 |

**If Stormwater Enters the LS-VFS from a BMP**

|  |           |          |
|--|-----------|----------|
| Type of BMP  | Pick one: |          |
| Peak discharge from the BMP during the design storm  |           | cfs      |
| Peak discharge from the BMP during the 10-year storm |           | cfs      |
| Maximum capacity of a 100-foot long LS-VFS           | 10        | cfs      |
| Peak flow directed to the LS-VFS                     |           | cfs      |
| Is a flow bypass system going to be used?            |           | (Y or N) |
| Explanation of any "Other" responses above           |           |          |

*Do not complete this section of the form.*

*Do not complete this section of the form.*

*Do not complete this section of the form.*

**LS-VFS Design**

|   |     |        |                              |
|---|-----|--------|------------------------------|
| Forebay surface area                            | 400 | sq ft  | Forebay is adequately sized. |
| Depth of forebay at stormwater entry point      | 24  | in     | Depth is appropriate.        |
| Depth of forebay at stormwater exit point       | 6   | in     | Depth is appropriate.        |
| Feet of level lip needed per cfs                | 10  | ft/cfs |                              |
| Computed minimum length of the level lip needed | 30  | ft     |                              |

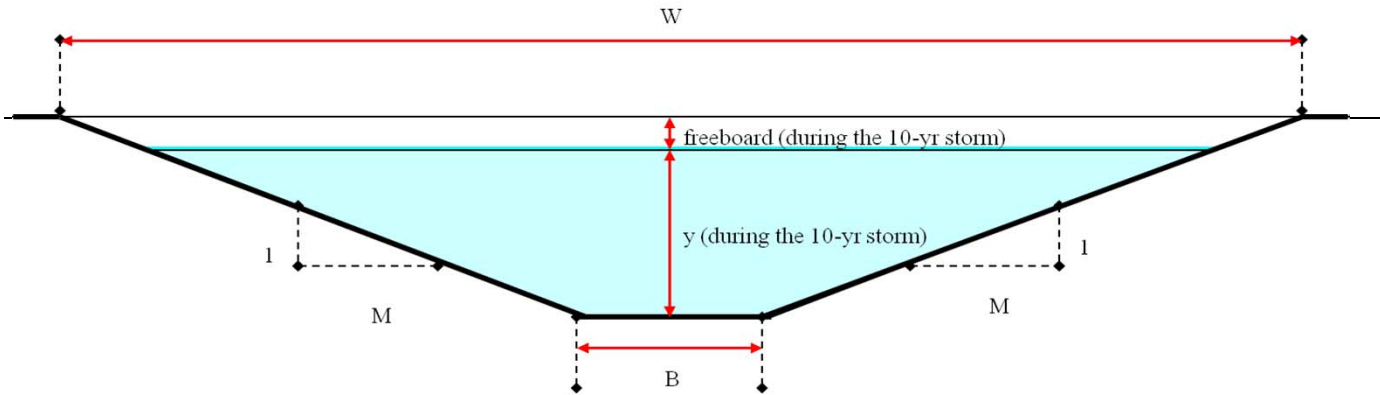
|  |        |             |
|--|--------|-------------|
| Length of level lip provided                                 | 50     | ft          |
| Width of VFS   | 30     | ft          |
| Elevation at downslope base of level lip                     | 446.25 | fmsl        |
| Elevation at the end of the VFS that is farthest from the LS | 444.75 | fmsl        |
| Slope (from level lip to the end of the VFS)                 | 5.00   | %           |
| Are any draws present in the VFS?                            | N      | (Y or N) OK |
| Is there a collector swale at the end of the VFS?            | N      | (Y or N)    |

**Bypass System Design (if applicable)**

|   |   |   |
|---|---|---|
| Is a bypass system provided?                  | Y | (Y or N)  |
| Is there an engineered flow splitting device? | Y | (Y or N) Please provide plan details of flow splitter & supporting calcs. |

Dimensions of the channel (see diagram below):

|   |                  |          |
|---|------------------|----------|
| M   | Existing Channel | ft       |
| B   |                  | ft       |
| W   |                  | ft       |
| y (flow depth for 10-year storm)                    |                  | ft       |
| freeboard (during the 10-year storm)                |                  | ft       |
| Peak velocity in the channel during the 10-yr storm | 9.16             | ft/sec   |
| Channel lining material                             | Pick one:        |          |
| Does the bypass discharge through a wetland?        | N                | (Y or N) |
| Does the channel enter the stream at an angle?      | Y                | (Y or N) |
| Explanation of any "Other" responses above          |                  |          |



**III. REQUIRED ITEMS CHECKLIST**

EDIT Please indicate the page or plan sheet numbers where the supporting documentation can be found. An incomplete submittal package will result in a request for additional information. This will delay final review and approval of the project. Initial in the space provided to indicate the following design requirements have been met. If the applicant has designated an agent, the agent may initial below. If a requirement has not been met, attach justification.

Required Item:

- Plans (1" - 50' or larger) of the entire site showing:
  - Design at ultimate build-out,
  - Off-site drainage (if applicable),
  - Delineated drainage basins (include Rational C coefficient per basin),
  - Forebay (if applicable),
  - High flow bypass system,
  - Maintenance access,
  - Proposed drainage easement and public right of way (ROW), and
  - Boundaries of drainage easement.

| Initials | Page or plan sheet number and any notes: |
|----------|--|
| GCA      | C3.2-C3.3                                |



2. Plan details (1" = 30' or larger) for the level spreader showing:
  - Forebay (if applicable),
  - High flow bypass system,
  - One foot topo lines between the level lip and top of stream bank,
  - Proposed drainage easement, and
  - Design at ultimate build-out.
  
3. Section view of the level spreader (1" = 20' or larger) showing:
  - Underdrain system (if applicable),
  - Level lip,
  - Upslope channel, and
  - Downslope filter fabric.
  
4. Plan details of the flow splitting device and supporting calculations (if applicable).
  
5. A construction sequence that shows how the level spreader will be protected from sediment until the entire drainage area is stabilized.
  
6. If a non-engineered VFS is being used, then provide a photograph of the VFS showing that no draws are present.
  
7. The supporting calculations.
  
8. A copy of the signed and notarized operation and maintenance (O&M) agreement.

|            |                                  |
|------------|----------------------------------|
| <u>GCA</u> | D4.4                             |
| <u>GCA</u> | D4.4                             |
|            | D4.4                             |
| <u>GCA</u> | C3.2-C3.3                        |
|            | N/A                              |
| <u>GCA</u> | Narrative & calculations booklet |
| <u>GCA</u> | Included                         |



North Carolina Department of Environment and Natural Resources

Division of Water Quality

Charles Wakild, P. E.

Director

Pat McCrory  
Governor

John E. Skvarla, III  
Secretary

January 14, 2013

DWQ Project # 05-0732v25  
Chatham County

Mr. Bill Mumford, Assistant Vice President  
NNP – Briar Chapel LLC  
16 Windy Knoll Circle  
Chapel Hill, NC 27516

Subject Property: **Briar Chapel, Great Ridge Parkway Extension**

## **APPROVAL OF MODIFIED STORMWATER PLAN**

Dear Mr. Mumford:

On January 11, 2008, the Division of Water Quality (DWQ) issued a revised 401 Water Quality Certification to temporarily impact 339 linear feet of stream and 0.157 acre of 404 wetlands and to permanently impact 1,666 linear feet of stream and 0.159 acre of 404 wetland in order to construct the Briar Chapel Subdivision in Chatham County.

In order to meet Condition 10 of the 401 Certification for this project, a stormwater management plan for Briar Chapel – Great Ridge Parkway Extension, dated December 18, 2012, was received on December 20, 2012.

The DWQ approves the SMP as satisfying Condition 10 of the General Water Quality Certification. This approval is for the purpose and design that you described in your application. If you change your project, you must notify us and you may be required to send us a new SMP. This approval requires to you follow the conditions listed in the General Water Quality Certification for the project and the following additional conditions listed below:

1. The SMP approved by the DWQ consists of one (1) wet detention pond and one (1) Level Spreader-Engineered Filter Strip and all associated stormwater conveyances, inlet and outlet strictures, and the grading and drainage patterns depicted on plan sheets dated December 19, 2012. The plans and specifications for the Great Ridge Parkway Extension approved by DWQ are incorporated by reference into this approval and are enforceable by DWQ provided however that any modification of the design for the stormwater management system that is accepted by DWQ shall take precedence over the original plans and specifications.

2. The maximum allowable drainage area for the approved wet detention pond shall be 1,705,452 square feet and the maximum allowable built-upon area within that drainage area shall be 1,117,211 square feet. The maximum allowable drainage area for the Level Spreader-Engineered Filter Strip shall be 147,452 square feet and the maximum allowable built-upon area within that drainage area shall be 62,438 square feet. Built-upon area includes, but is not limited to, roofed structures, asphalt, concrete, gravel, brick, slate, coquina and parking areas, but does not include raised, uncovered open slat decking or the water surface of swimming pools. Any changes to these maximum areas shall require the applicant to submit and receive approval for a revised stormwater management plan by the DWQ.
3. The footprint of all stormwater management devices as well as an additional 10-foot wide area on all sides of the devices shall be located in public rights-of-way, dedicated common areas or recorded easement areas. The final plats for the project showing all such rights-of-way, common areas and easement areas shall be in accordance with the approved plans.
4. Maintenance activities for the wet detention pond shall be performed in accordance with the notarized O&M agreements signed by Kevin Graham (Vice President, Operations) on December 13, 2012. The O&M agreement must transfer with the sale of the land or transfer of ownership/responsibility for the BMP facility. DWQ must be notified promptly of every transfer.
5. The applicant and/or authorized agent shall provide a completed Certificate of Completion form to the DWQ within thirty (30) days of project completion (available at <http://portal.ncdenr.org/web/wq/swp/ws/401/certsandpermits/apply/forms>).

Thank you for your attention to this matter. If you have any questions or wish to discuss these matters further, please do not hesitate to contact me at (919) 807-6381.

Sincerely,



Annette Lucas, P.E.  
Wetlands, Buffers and Stormwater Compliance and  
Permitting (Webscape) Unit

AML/aml

Cc: Becky Fox, EPA  
USACE, Raleigh  
DWQ Raleigh Regional Office  
Chatham County Public Works Dept., P.O. Box 1550, Pittsboro, NC 27312  
File Copy