

BRIAR CHAPEL – PHASE 6 NORTH

Chatham County, North Carolina

FINAL STORMWATER MANAGEMENT PLAN DESIGN CALCULATIONS

Project Number:	NEW-12000
Designed By:	Jeremy V. Finch, PE
Date:	June 2012
NC LIC:	#C-2093



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RESEARCH TRIANGLE PARK

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LIMITED LIABILITY COMPANY ANNUAL REPORT

E-Filed Annual Report
-1-0-5468752

Do not data enter manually.

NAME OF LIMITED LIABILITY COMPANY: *NNP-Briar Chapel, LLC*

STATE OF INCORPORATION: *DE*

SECRETARY OF STATE L.L.C. ID NUMBER: *0631973*

NATURE OF BUSINESS: *Real Estate Development*

REGISTERED AGENT: *National Registered Agents, Inc.*

REGISTERED OFFICE MAILING ADDRESS: *120 Penmarc Drive
Raleigh, NC 27603*

REGISTERED OFFICE STREET ADDRESS: *120 Penmarc Drive
Raleigh, NC 27603 Wake County*

PRINCIPAL OFFICE TELEPHONE NUMBER: *8584557503*

PRINCIPAL OFFICE MAILING ADDRESS: *9820 Towne Centre Drive Suite 100
San Diego, CA 92121*

PRINCIPAL OFFICE STREET ADDRESS: *9820 Towne Centre Drive Suite 100
San Diego, CA 92121*

MANAGERS/MEMBERS/ORGANIZERS:

*Name: Newland National Partners, LP
Title: Manager
Address:
9820 Towne Centre Drive Suite 100
San Diego, CA 92121*

CERTIFICATION OF ANNUAL REPORT MUST BE COMPLETED BY ALL LIMITED LIABILITY COMPANIES

Newland National Partners, LP

04/15/2011

FORM MUST BE SIGNED BY A MANAGER/MEMBER

DATE

Dolores A Valle

Manager

TYPE OR PRINT NAME

TYPE OR PRINT TITLE

ANNUAL REPORT FEE: \$200 MAIL TO: Secretary of State • Corporations Division • Post Office Box 29525 • Raleigh, NC 27626-0525



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BRIAR CHAPEL – PHASE 6 NORTH

CHATHAM COUNTY, NORTH CAROLINA

FINAL STORMWATER MANAGEMENT PLAN DESIGN

NEW-12000



June 2012

Jeremy V. Finch, PE
Project Manager

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Design Services Focused On Client Success

BRIAR CHAPEL – PHASE 6 NORTH
Final Stormwater Management Plan Design

General Description

Located off of US Highway 15-501, north of Andrews Store Road and south of Mann's Chapel Road in Chatham County, NC is the proposed development known as Briar Chapel. Phase 6 North of the proposed development is approximately 37-acres and will consist of the construction of single-family lots along with the associated utility, parking, and roadway infrastructure.

The overall proposed Briar Chapel development is located within the Cape Fear River Basin, and drains to a stream (Pokeberry Creek) classified as Water Supply IV (WS-IV), and Nutrient Sensitive Waters (NSW). As a result of the proposed development exceeding the maximum allowable limit for stream impacts, an individual permit issued by The United States Army Corps of Engineers (USACE) was required (Clean Water Act Section 404 permit). Also, a Clean Water Act Section 401 Water Quality Certification from NCDWQ was attached to the individual permit. Under the 401 Water Quality Certification issued by NCDWQ, the proposed site will be required to comply with the following stormwater management requirements:

- 1. A final written stormwater management plan for each subwatershed (including signed and notarized Operation and Maintenance agreements) shall be submitted to the 401 Oversight and Express Permitting Unit. The stormwater management plan may be submitted to DWQ in phases for written approval as long as no impact to wetlands or streams occur in that phase until written approval is received from DWQ.*
- 2. The stormwater plans shall utilize constructed wetlands, bioretention areas, wet ponds followed by forested filter strips and similar best management practices designed to remove nutrients. The stormwater management plan must include plans, specifications, and worksheets for stormwater management facilities that are appropriate for the surface water classification and designed to remove at least 85% TSS according to the most recent version of the NCDENR Stormwater Best Management Practices Manual.*
- 3. For low density areas of the project with low impervious surface area, engineered stormwater management facilities are not expected. For these areas of lower impervious area, similar best management practices that remove nutrients such as grassed swales and vegetated riparian buffers should be sufficient rather than more intensive engineered stormwater devices such as constructed wetlands.*

In addition to the above DWQ stormwater requirements, the following stormwater quality and quantity items are required per Section 8.3 ("Stormwater Controls") of the Chatham County Compact Communities Ordinance:

- 1. Control and treat the first inch of runoff from the project site and from any offsite drainage routed to an on-site control structure. Ensure that the draw down time for this treatment volume is a minimum of forty eight (48) hours and a maximum of one hundred and twenty (120) hours.*
- 2. Maintain the discharge rate for the treatment volume at or below the pre-development discharge rate for the 1-year, 24-hour storm.*

The proposed stormwater management plan for Phase 6 North of Briar Chapel will be designed to protect the downstream environment. The plan incorporates biologically based stormwater management techniques to manage both water quantity and quality aspects of site runoff. As can be seen in this report, stormwater

management for Phase 6 North will be accomplished by incorporating an engineered stormwater best management practice facility to capture and treat the stormwater runoff from developed areas. The specific stormwater treatment device that will be used is a wet detention basin designed to remove a minimum of 90% average annual total suspended solids (TSS), provide slow release (i.e. 2 to 5 days) of the difference in pre- to post-development peak runoff rate for the 1-year, 24-hour storm. This report contains the final design calculations for the proposed wet detention basin located in Phase 6 North of Briar Chapel. Please refer to the summary of results and discussion of results sections of this report for additional information.

Calculation Methodology

- Rainfall data for the Chatham County, NC region is from NOAA Atlas 14, with a partial duration series assumption. The rainfall depths were entered into a spreadsheet that calculated a center-weighted storm based upon the NOAA Atlas 14 depths. The 1-year/24-hour rainfall depth is 2.95 inches, the 2-Year/24-hour rainfall depth is 3.56 inches, the 10-Year/24-hour rainfall depth is 5.16 inches, and the 100-year/24-hour rainfall depth is 7.62 inches. All of these “computed” storms were modeled within the hydrologic model. Please reference the rainfall data section within this report for additional information.
- Using maps contained within the Chatham County Soil Survey, the watershed soils were determined to be from hydrologic soil group (HSG) ‘B’ soils. Since the method chosen to compute the post-development peak flow rates and runoff volumes is dependent upon the soil type, all hydrologic calculations are based upon the assumption of HSG ‘B’ soils.
- A composite SCS Curve Number was calculated for the post-development condition using SCS curve numbers and land cover conditions. Land cover conditions for the post-development condition were taken from the proposed development plan.
- The post-development time of concentration to the wet detention basin was assumed to be 5 minutes in the post-development condition.
- All on-site topo was taken from a flown aerial topographic survey by others provided to The John R. McAdams Company, Inc. by McKim & Creed. The drainage map for the post-development condition has been included in this report.
- PondPack Version V8i, by Haestad Methods, was used to generate post-development peak flow rates and generate the stage-discharge rating curve for the proposed wet detention basin. Final routing calculations for the wet detention basin were also performed within Pondpack.
- The stage-storage rating curve and stage-storage function for the proposed wet detention basin was generated externally in a spreadsheet and then input into Pondpack.
- A velocity dissipater is provided at the end of the principal spillway outlet for the wet detention basin to prevent erosion and scour in the downstream area. The dissipater is constructed using riprap, underlain with a woven geotextile filter fabric. The filter fabric is used to minimize the loss of soil particles beneath the riprap apron. The dissipater is sized for the 10-year storm event using the NYDOT method. It is a permanent feature of the outlet.
- Water quality sizing calculations for each facility were performed in accordance with the N.C. Stormwater Best Management Practices manual (NCDENR July 2007). The wet detention basin surface area was sized by multiplying the drainage area to the facility by the interpolated SA/DA ratio from the *Surface Area to Drainage Area Ratio for Permanent Pool Sizing to Achieve 90% TSS Pollutant Removal Efficiency in the Mountain & Piedmont Regions*. The minimum temporary pool volume was determined by calculating the 1-inch runoff volume using the Simple Method.

Conclusion

If the development on this tract is built as proposed within this report, then the requirements set forth in the Water Quality Certification #3402 (WQC #3402) and Section 8.3 ("Stormwater Controls") of the Chatham County Compact Communities Ordinance will be met with the proposed wet detention basin. However, modifications to the proposed development may require that this analysis be revised. Some modifications that would **require** this analysis to be revised include:

1. The proposed site impervious surface exceeds the amount accounted for in this report.
2. The post-development watershed breaks change significantly from those used to prepare this report.

The above modifications may result in the assumptions within this report becoming invalid. The computations within this report will need to be revisited if any of the above conditions become apparent as development of the proposed site moves forward.

1	SUMMARY OF RESULTS
2	USGS MAP
3	SOILS INFORMATION
4	FEMA FIRM PANEL MAP
5	RAINFALL INFORMATION
6	HYDROLOGIC CALCULATIONS
7	WET POND FINAL DESIGN CALCULATIONS

SUMMARY OF RESULTS

SUMMARY OF RESULTS

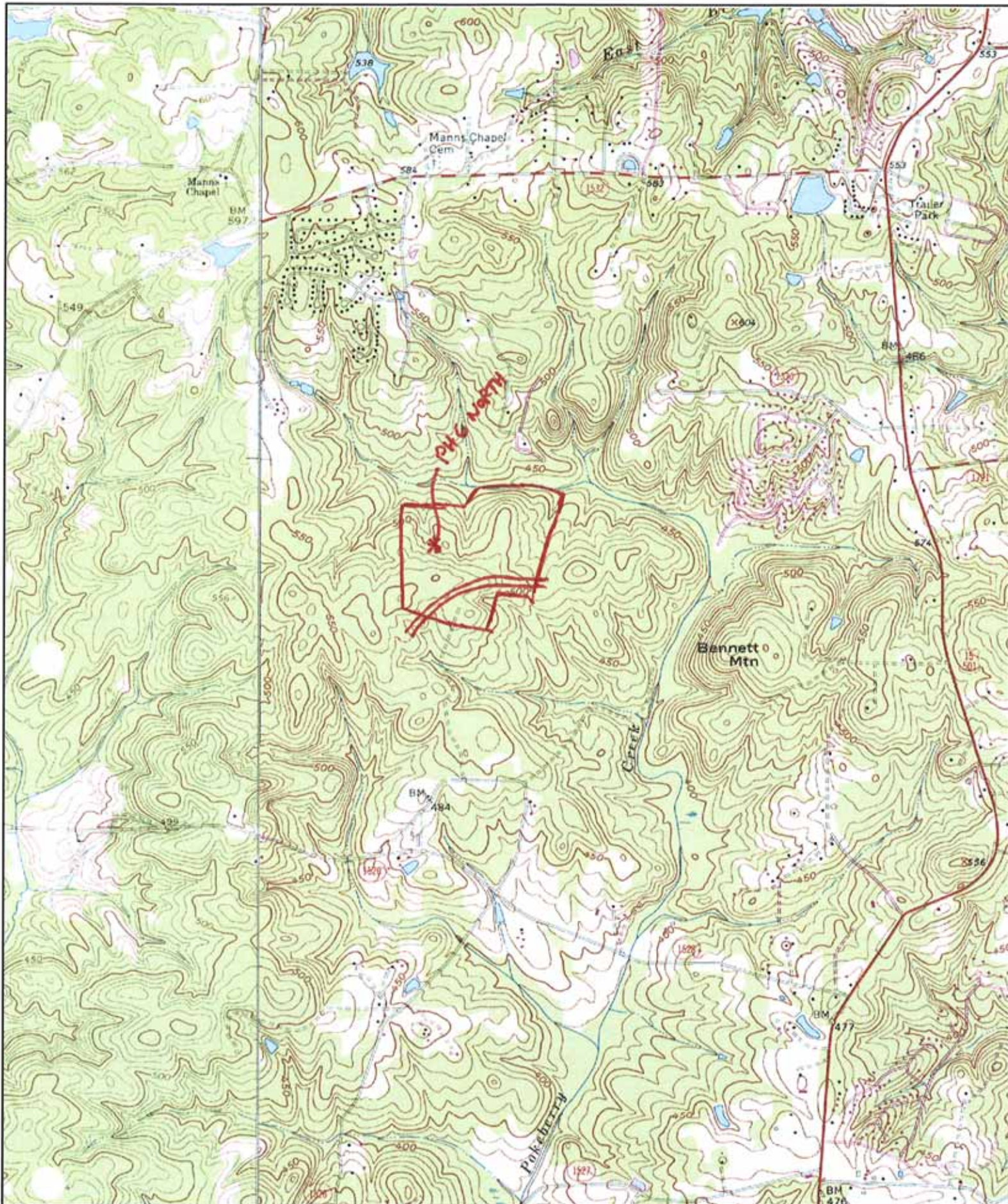
WET POND

Return Period	Inflow [cfs]	Outflow [cfs]	Max. WSE [ft]	Freeboard [ft]
1-Year	43.46	0.36	474.39	2.61
2-Year	60.48	2.20	474.60	2.40
10-Year	96.67	24.41	475.04	1.96
25-Year	114.39	50.33	475.38	1.62
100-Year	138.31	70.98	475.94	1.06

Design Drainage Area =	20.69	acres
Design Impervious Area =	10.26	acres
% Impervious =	49.6%	
Top of Dam =	477.00	ft
Normal Pool Elevation =	472.00	ft
Surface Area at NWSE =	25,869	sf
Minimum Required Surface Area at NWSE =	23,085	sf
Water Quality Volume Storage Provided =	80,105	cf
Minimum Required Water Quality Volume Storage =	37,264	cf
Design Drawdown Time =	2.62	days
Riser Length =	5	ft
Riser Width =	5	ft
Riser Crest =	474.50	ft
Barrel Diameter =	30	inches
# of Barrels =	1	
Invert In =	466.00	feet
Invert Out =	462.00	feet
Length =	83	feet
Slope =	0.0482	ft/ft

USGS MAP

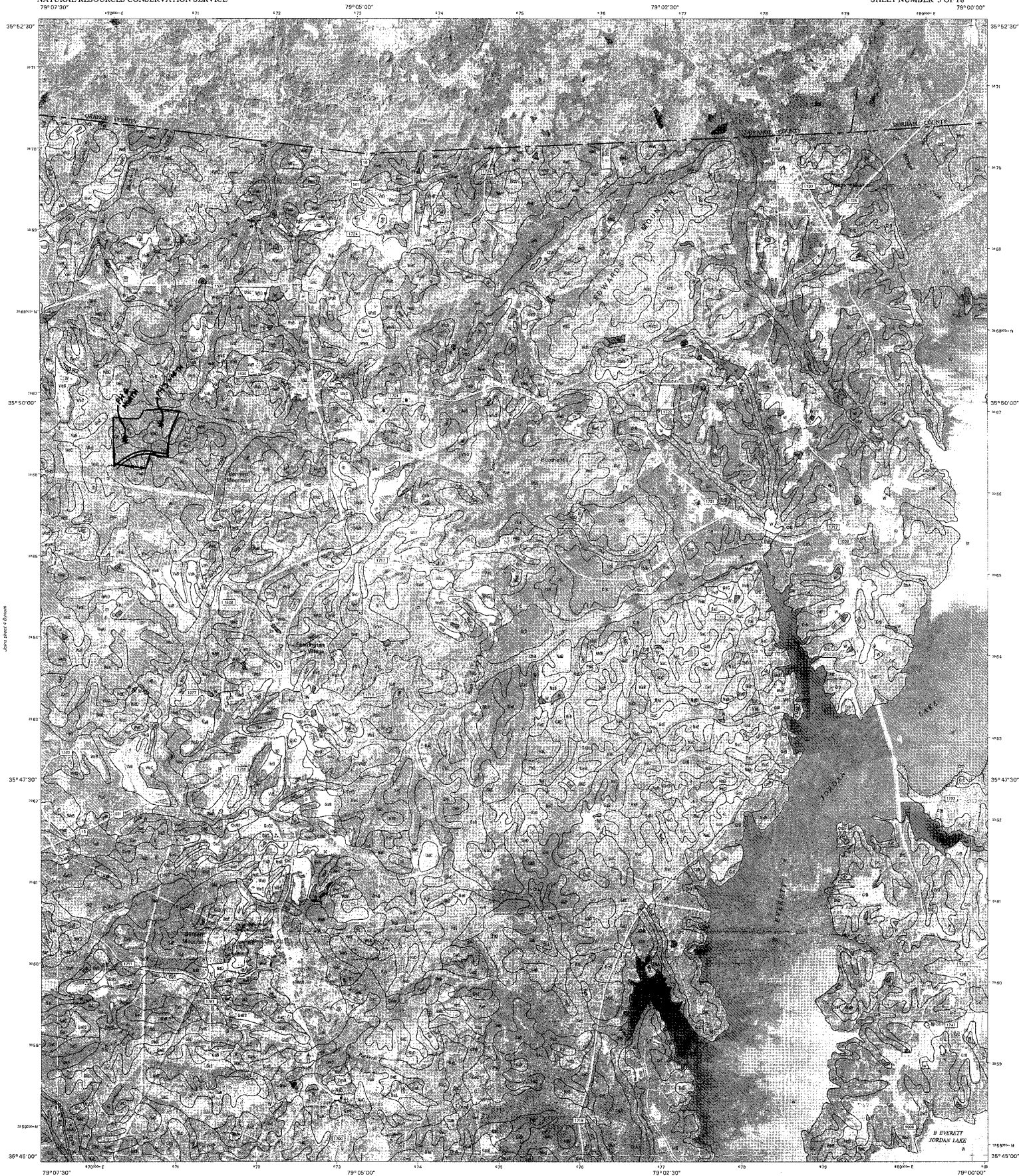
BRIAR CHAPEL – PHASE 6 NORTH
NEW-12000



Name: m:\NC3pro\35079G1A.P24
Date: 3/15/2012
Scale: 1 inch equals 2000 feet

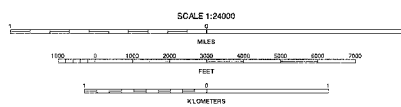
Location: 035° 49' 36.37" N 079° 06' 41.37" W

SOILS INFORMATION



This soil survey was compiled by the U.S. Department of Agriculture, Natural Resources Conservation Service and cooperating agencies. Base maps are orthophotographs prepared by the U.S. Department of the Interior, Geological Survey, from 1973-1999 aerial photography. Administrative boundaries were adopted from the State of North Carolina. Boundaries may have been edited to conform with features represented on the publication orthophotography or to enhance the clarity of the soils information.

North American Datum of 1983 (NAD83), GRS80 Spheroid
1000-meter UTM Universal Transverse Mercator, zone 17.
Coordinate grid lines and grid section data, if shown, are approximately positioned. Digital data are available for this quadrangle.



4	5	6
10	11	12

BACK TO ADJOINING 7.5 MAPS

- 4 BROWN
- 5 GREEN LEVEL
- 10 PITCHING
- 11 BERRY OAKS
- 12 HUNTER

FARRINGTON, NORTH CAROLINA
7.5 MINUTE SERIES
SHEET NUMBER 5 OF 18

Soil map delineations extending beyond the dashed white quadrangle outline are for reference only and are included on adjacent map sheets.

FEMA FIRM PANEL MAP

**BRIAR CHAPEL – PHASE 6 NORTH
NEW-12000**

DATE OF INFORMATION The information used in this advertisement is as of the date shown above.	
NAME OF THE COMPANY The name of the company is as shown above.	
NAME OF THE PRODUCT The name of the product is as shown above.	
NAME OF THE MANUFACTURER The name of the manufacturer is as shown above.	
NAME OF THE DISTRIBUTOR The name of the distributor is as shown above.	
NAME OF THE RETAILER The name of the retailer is as shown above.	
NAME OF THE WHOLESALE The name of the wholesaler is as shown above.	
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All answers listed in the Speed-Related Data Table were selected by selected nations only, but surveys (like Speed-Related Data Table) as they may not have been selected along with a correct answer or correct answer. Nations provide this information in the Speed-Related Data Table as they may be contained in the Speed-Related Data Table.

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The use of a 10% to 20% reduction in the number of people in the room is recommended. The use of a 10% to 20% reduction in the number of people in the room is recommended. The use of a 10% to 20% reduction in the number of people in the room is recommended.

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There seems to be the opportunity (which indeed has, in numerous cases, been seized) for the National Trust to make a more effective use of its resources. It is not clear, for example, why the National Trust should have been asked to take on the management of the National Trust for Wales, or why it should have been asked to take on the management of the National Trust for Scotland. It is not clear, for example, why the National Trust should have been asked to take on the management of the National Trust for Wales, or why it should have been asked to take on the management of the National Trust for Scotland. It is not clear, for example, why the National Trust should have been asked to take on the management of the National Trust for Wales, or why it should have been asked to take on the management of the National Trust for Scotland.

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RAINFALL INFORMATION

Center Weighted Storm Computation - Based on NOAA Atlas 14 Results

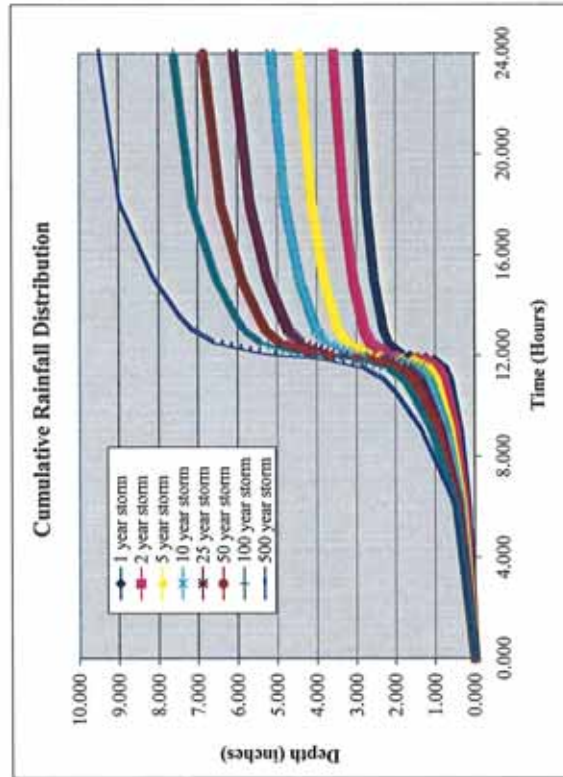
Copy input data from NOAA Atlas 14:

- 1) Have NOAA Atlas 14 results in Internet Explorer Window
- 2) Copy from ARI of one year to 1000 year, 60 day precipitation value. Do not include column headings. "1" will be in upper left of selection, 1000-yr; 60-day result in lower right of selection.
- 3) Paste with starting point at ARI of 1 year (first cell in the ARI column, cell A12). Cannot paste special to preserve format, format is via macro in next step
- 4) Place cursor on ARI of 1 year (cell A12), and press CTRL+V for format - make sure that A12 is the only cell selected before running the format macro.
- 5) Copy results of output data (below rainfall input) into PondPack

ARI (years)	5	10	15	30	60	120	3	6	12	24	48	4	7	10	20	30	45	60
1	0.41	0.66	0.83	1.14	1.42	1.68	1.79	2.15	2.54	2.95	3.45	3.65	3.85	4.43	5.04	6.76	8.38	10.68
2	0.49	0.78	0.98	1.36	1.71	2.03	2.16	2.59	3.06	3.56	4.15	4.39	4.62	5.29	5.99	7.97	9.86	12.51
5	0.56	0.9	1.14	1.63	2.08	2.51	2.68	3.21	3.81	4.46	5.15	5.42	5.69	6.43	7.2	9.41	11.46	14.31
10	0.62	0.99	1.26	1.82	2.37	2.88	3.09	3.72	4.44	5.16	5.93	6.23	6.53	7.33	8.14	10.55	12.7	15.71
25	0.68	1.09	1.38	2.04	2.72	3.34	3.62	4.38	5.28	6.1	6.97	7.32	7.67	8.56	9.41	12.1	14.34	17.53
50	0.72	1.15	1.46	2.2	2.98	3.71	4.05	4.92	5.97	6.85	7.79	8.18	8.56	9.54	10.41	13.32	15.59	18.92
100	0.76	1.21	1.53	2.35	3.23	4.06	4.47	5.46	6.69	7.62	8.63	9.05	9.48	10.54	11.42	14.55	16.84	20.27
200	0.79	1.26	1.59	2.47	3.47	4.41	4.89	6.02	7.44	8.4	9.48	9.96	10.43	11.56	12.45	15.8	18.09	21.62
500	0.83	1.31	1.65	2.62	3.77	4.86	5.46	6.78	8.48	9.49	10.66	11.19	11.73	12.97	13.85	17.51	19.76	23.4
1000	0.85	1.35	1.69	2.74	4	5.22	5.93	7.41	9.36	10.34	11.58	12.17	12.76	14.09	14.95	18.85	21.04	24.75

Output Data to Export to PondPack, 5 minute intervals

Time (min)	Time (hours)	1 year (min)	2 year (min)	5 year (min)	10 year (min)	25 year (min)	50 year (min)	100 year (min)	500 year (min)
0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5	0.083	0.003	0.003	0.005	0.005	0.006	0.006	0.006	0.007
10	0.167	0.006	0.007	0.009	0.010	0.011	0.012	0.013	0.014
15	0.250	0.009	0.010	0.014	0.015	0.017	0.018	0.019	0.021
20	0.333	0.011	0.014	0.018	0.020	0.023	0.024	0.026	0.028
25	0.417	0.014	0.017	0.023	0.025	0.028	0.031	0.032	0.035
30	0.500	0.017	0.021	0.027	0.030	0.034	0.037	0.039	0.042
35	0.583	0.020	0.024	0.032	0.035	0.040	0.043	0.045	0.049
40	0.667	0.023	0.028	0.036	0.040	0.046	0.049	0.052	0.056
45	0.750	0.026	0.031	0.041	0.045	0.051	0.055	0.058	0.063
50	0.833	0.028	0.035	0.045	0.050	0.057	0.061	0.065	0.070
55	0.917	0.031	0.038	0.050	0.055	0.063	0.067	0.071	0.077
60	1.000	0.034	0.042	0.054	0.060	0.068	0.073	0.078	0.084
65	1.083	0.037	0.045	0.059	0.065	0.074	0.079	0.084	0.091
70	1.167	0.040	0.049	0.063	0.070	0.080	0.086	0.090	0.098
75	1.250	0.043	0.052	0.068	0.075	0.085	0.092	0.097	0.105
80	1.333	0.046	0.056	0.072	0.080	0.091	0.098	0.103	0.112
85	1.417	0.048	0.059	0.077	0.085	0.097	0.104	0.110	0.119
90	1.500	0.051	0.063	0.081	0.090	0.103	0.110	0.116	0.126
95	1.583	0.054	0.066	0.086	0.095	0.108	0.116	0.123	0.133
100	1.667	0.057	0.069	0.090	0.100	0.114	0.122	0.129	0.140
105	1.750	0.060	0.073	0.095	0.105	0.120	0.128	0.136	0.147
110	1.833	0.063	0.076	0.099	0.110	0.125	0.134	0.142	0.154
115	1.917	0.065	0.080	0.104	0.115	0.131	0.141	0.149	0.161
120	2.000	0.068	0.083	0.108	0.120	0.137	0.147	0.155	0.168



Output Data to Export to PondPack, 5 minute intervals

Time (min)	Time (hours)	1 year (min)	2 year (min)	5 year (min)	10 year (min)	25 year (min)	50 year (min)	100 year (min)	500 year (min)
125	2.083	0.071	0.087	0.113	0.125	0.142	0.153	0.161	0.175
130	2.167	0.074	0.090	0.117	0.130	0.148	0.159	0.168	0.182
135	2.250	0.077	0.094	0.122	0.135	0.154	0.165	0.174	0.189
140	2.333	0.080	0.097	0.126	0.140	0.159	0.171	0.181	0.196
145	2.417	0.083	0.101	0.131	0.145	0.165	0.177	0.187	0.203
150	2.500	0.085	0.104	0.135	0.150	0.171	0.183	0.194	0.210
155	2.583	0.088	0.108	0.140	0.155	0.177	0.189	0.200	0.217
160	2.667	0.091	0.111	0.144	0.160	0.182	0.196	0.207	0.224
165	2.750	0.094	0.115	0.149	0.165	0.188	0.202	0.213	0.231
170	2.833	0.097	0.118	0.153	0.170	0.194	0.208	0.220	0.238
175	2.917	0.100	0.122	0.158	0.175	0.199	0.214	0.226	0.245
180	3.000	0.103	0.125	0.163	0.180	0.205	0.220	0.233	0.253
185	3.083	0.105	0.128	0.167	0.185	0.211	0.226	0.239	0.260
190	3.167	0.108	0.132	0.172	0.190	0.216	0.232	0.245	0.267
195	3.250	0.111	0.135	0.176	0.195	0.222	0.238	0.252	0.274
200	3.333	0.114	0.139	0.181	0.200	0.228	0.244	0.258	0.281
205	3.417	0.117	0.142	0.185	0.205	0.233	0.251	0.265	0.288
210	3.500	0.120	0.146	0.190	0.210	0.239	0.257	0.271	0.295
215	3.583	0.122	0.149	0.194	0.215	0.245	0.263	0.278	0.302
220	3.667	0.125	0.153	0.199	0.220	0.251	0.269	0.284	0.309
225	3.750	0.128	0.156	0.203	0.225	0.256	0.275	0.291	0.316
230	3.833	0.131	0.160	0.208	0.230	0.262	0.281	0.297	0.323
235	3.917	0.134	0.163	0.212	0.235	0.268	0.287	0.304	0.330
240	4.000	0.137	0.167	0.217	0.240	0.273	0.293	0.310	0.337
245	4.083	0.140	0.170	0.221	0.245	0.279	0.299	0.316	0.344
250	4.167	0.142	0.174	0.226	0.250	0.285	0.306	0.323	0.351
255	4.250	0.145	0.177	0.230	0.255	0.290	0.312	0.329	0.358
260	4.333	0.148	0.181	0.235	0.260	0.296	0.318	0.336	0.365
265	4.417	0.151	0.184	0.239	0.265	0.302	0.324	0.342	0.372
270	4.500	0.154	0.188	0.244	0.270	0.308	0.330	0.349	0.379
275	4.583	0.157	0.191	0.248	0.275	0.313	0.336	0.355	0.386
280	4.667	0.159	0.194	0.253	0.280	0.319	0.342	0.362	0.393
285	4.750	0.162	0.198	0.257	0.285	0.325	0.348	0.368	0.400
290	4.833	0.165	0.201	0.262	0.290	0.330	0.354	0.375	0.407
295	4.917	0.168	0.205	0.266	0.295	0.336	0.361	0.381	0.414
300	5.000	0.171	0.208	0.271	0.300	0.342	0.367	0.388	0.421
305	5.083	0.174	0.212	0.275	0.305	0.347	0.373	0.394	0.428
310	5.167	0.177	0.215	0.280	0.310	0.353	0.379	0.400	0.435
315	5.250	0.179	0.219	0.284	0.315	0.359	0.385	0.407	0.442
320	5.333	0.182	0.222	0.289	0.320	0.364	0.391	0.413	0.449
325	5.417	0.185	0.226	0.293	0.325	0.370	0.397	0.420	0.456
330	5.500	0.188	0.229	0.298	0.330	0.376	0.403	0.426	0.463
335	5.583	0.191	0.233	0.302	0.335	0.382	0.409	0.433	0.470
340	5.667	0.194	0.236	0.307	0.340	0.387	0.416	0.439	0.477
345	5.750	0.196	0.240	0.311	0.345	0.393	0.422	0.446	0.484
350	5.833	0.199	0.243	0.316	0.350	0.399	0.428	0.452	0.491
355	5.917	0.202	0.247	0.320	0.355	0.404	0.434	0.459	0.498
360	6.000	0.205	0.250	0.325	0.360	0.410	0.440	0.465	0.505

Output Data to Export to PondPack, 5 minute intervals

Time (min)	Time (hours)	1 year (min)	2 year (min)	5 year (min)	10 year (min)	25 year (min)	50 year (min)	100 year (min)	500 year (min)
365	6.083	0.210	0.257	0.333	0.370	0.422	0.455	0.482	0.529
370	6.167	0.216	0.263	0.342	0.380	0.435	0.469	0.499	0.552
375	6.250	0.221	0.270	0.350	0.390	0.447	0.484	0.516	0.576
380	6.333	0.227	0.276	0.358	0.400	0.460	0.498	0.533	0.599
385	6.417	0.232	0.283	0.367	0.410	0.472	0.513	0.550	0.623
390	6.500	0.238	0.289	0.375	0.420	0.485	0.528	0.568	0.647
395	6.583	0.243	0.296	0.383	0.430	0.497	0.542	0.585	0.670
400	6.667	0.248	0.302	0.392	0.440	0.510	0.557	0.602	0.694
405	6.750	0.254	0.309	0.400	0.450	0.522	0.571	0.619	0.718
410	6.833	0.259	0.315	0.408	0.460	0.535	0.586	0.636	0.741
415	6.917	0.265	0.322	0.417	0.470	0.547	0.600	0.653	0.765
420	7.000	0.270	0.328	0.425	0.480	0.560	0.615	0.670	0.788
425	7.083	0.275	0.335	0.433	0.490	0.572	0.630	0.687	0.812
430	7.167	0.281	0.341	0.442	0.500	0.585	0.644	0.704	0.836
435	7.250	0.286	0.348	0.450	0.510	0.597	0.659	0.721	0.859
440	7.333	0.292	0.354	0.458	0.520	0.610	0.673	0.738	0.883
445	7.417	0.297	0.361	0.467	0.530	0.622	0.688	0.755	0.906
450	7.500	0.303	0.368	0.475	0.540	0.635	0.703	0.773	0.930
455	7.583	0.308	0.374	0.483	0.550	0.647	0.717	0.790	0.954
460	7.667	0.313	0.381	0.492	0.560	0.660	0.732	0.807	0.977
465	7.750	0.319	0.387	0.500	0.570	0.672	0.746	0.824	1.001
470	7.833	0.324	0.394	0.508	0.580	0.685	0.761	0.841	1.024
475	7.917	0.330	0.400	0.517	0.590	0.697	0.775	0.858	1.048
480	8.000	0.335	0.407	0.525	0.600	0.710	0.790	0.875	1.072
485	8.083	0.340	0.413	0.533	0.610	0.722	0.805	0.892	1.095
490	8.167	0.346	0.420	0.542	0.620	0.735	0.819	0.909	1.119
495	8.250	0.351	0.426	0.550	0.630	0.747	0.834	0.926	1.143
500	8.333	0.357	0.433	0.558	0.640	0.760	0.848	0.943	1.166
505	8.417	0.362	0.439	0.567	0.650	0.772	0.863	0.960	1.190
510	8.500	0.368	0.446	0.575	0.660	0.785	0.878	0.978	1.213
515	8.583	0.373	0.452	0.583	0.670	0.797	0.892	0.995	1.237
520	8.667	0.378	0.459	0.592	0.680	0.810	0.907	1.012	1.261
525	8.750	0.384	0.465	0.600	0.690	0.822	0.921	1.029	1.284
530	8.833	0.389	0.472	0.608	0.700	0.835	0.936	1.046	1.308
535	8.917	0.395	0.478	0.617	0.710	0.847	0.950	1.063	1.331
540	9.000	0.400	0.485	0.625	0.720	0.860	0.965	1.080	1.355
545	9.083	0.410	0.497	0.640	0.737	0.881	0.989	1.108	1.392
550	9.167	0.420	0.509	0.654	0.755	0.902	1.013	1.135	1.428
555	9.250	0.430	0.521	0.669	0.772	0.923	1.038	1.163	1.465
560	9.333	0.440	0.533	0.684	0.790	0.944	1.062	1.190	1.502
565	9.417	0.450	0.545	0.699	0.807	0.966	1.086	1.218	1.538
570	9.500	0.460	0.557	0.713	0.825	0.987	1.110	1.245	1.575
575	9.583	0.470	0.569	0.728	0.842	1.008	1.134	1.273	1.612
580	9.667	0.480	0.581	0.743	0.860	1.029	1.158	1.300	1.648
585	9.750	0.490	0.593	0.758	0.877	1.050	1.183	1.328	1.685
590	9.833	0.500	0.604	0.772	0.895	1.071	1.207	1.355	1.722
595	9.917	0.510	0.616	0.787	0.912	1.092	1.231	1.383	1.758
600	10.000	0.520	0.628	0.802	0.930	1.113	1.255	1.410	1.795

Output Data to Export to PondPack, 5 minute intervals

Time (min)	Time (hours)	1 year (min)	2 year (min)	5 year (min)	10 year (min)	25 year (min)	50 year (min)	100 year (min)	500 year (min)
605	10.083	0.530	0.640	0.816	0.947	1.134	1.279	1.438	1.832
610	10.167	0.540	0.652	0.831	0.965	1.156	1.303	1.465	1.868
615	10.250	0.550	0.664	0.846	0.982	1.177	1.328	1.493	1.905
620	10.333	0.560	0.676	0.861	1.000	1.198	1.352	1.520	1.942
625	10.417	0.570	0.688	0.875	1.018	1.219	1.376	1.548	1.978
630	10.500	0.580	0.700	0.890	1.035	1.240	1.400	1.575	2.015
635	10.583	0.589	0.711	0.904	1.053	1.263	1.428	1.609	2.065
640	10.667	0.598	0.722	0.918	1.070	1.287	1.457	1.643	2.115
645	10.750	0.608	0.733	0.933	1.088	1.310	1.485	1.678	2.165
650	10.833	0.617	0.743	0.947	1.105	1.333	1.513	1.712	2.215
655	10.917	0.626	0.754	0.961	1.123	1.357	1.542	1.746	2.265
660	11.000	0.635	0.765	0.975	1.140	1.380	1.570	1.780	2.315
665	11.083	0.657	0.792	1.011	1.183	1.432	1.631	1.849	2.406
670	11.167	0.678	0.818	1.047	1.225	1.483	1.692	1.918	2.497
675	11.250	0.700	0.845	1.083	1.268	1.535	1.753	1.988	2.588
680	11.333	0.722	0.872	1.118	1.310	1.587	1.813	2.057	2.678
685	11.417	0.743	0.898	1.154	1.353	1.638	1.874	2.126	2.769
690	11.500	0.765	0.925	1.190	1.395	1.690	1.935	2.195	2.860
695	11.583	0.831	1.006	1.294	1.518	1.839	2.104	2.384	3.096
700	11.667	0.896	1.087	1.399	1.642	1.988	2.273	2.573	3.331
705	11.750	0.962	1.168	1.503	1.765	2.137	2.442	2.762	3.567
710	11.833	1.027	1.249	1.608	1.888	2.286	2.611	2.951	3.802
715	11.917	1.237	1.494	1.898	2.208	2.636	2.981	3.336	4.212
720	12.000	1.647	1.984	2.458	2.828	3.316	3.701	4.096	5.042
725	12.083	1.857	2.229	2.748	3.148	3.666	4.071	4.481	5.452
730	12.167	1.923	2.311	2.852	3.272	3.814	4.239	4.669	5.688
735	12.250	1.988	2.392	2.957	3.395	3.963	4.408	4.858	5.923
740	12.333	2.054	2.473	3.061	3.518	4.112	4.577	5.047	6.159
745	12.417	2.119	2.554	3.166	3.642	4.261	4.746	5.236	6.394
750	12.500	2.185	2.635	3.270	3.765	4.410	4.915	5.425	6.630
755	12.583	2.207	2.662	3.306	3.807	4.462	4.976	5.494	6.721
760	12.667	2.228	2.688	3.342	3.850	4.513	5.037	5.563	6.812
765	12.750	2.250	2.715	3.378	3.892	4.565	5.098	5.633	6.903
770	12.833	2.272	2.742	3.413	3.935	4.617	5.158	5.702	6.993
775	12.917	2.293	2.768	3.449	3.977	4.668	5.219	5.771	7.084
780	13.000	2.315	2.795	3.485	4.020	4.720	5.280	5.840	7.175
785	13.083	2.324	2.806	3.499	4.037	4.743	5.308	5.874	7.225
790	13.167	2.333	2.817	3.513	4.055	4.767	5.337	5.908	7.275
795	13.250	2.343	2.828	3.528	4.072	4.790	5.365	5.943	7.325
800	13.333	2.352	2.838	3.542	4.090	4.813	5.393	5.977	7.375
805	13.417	2.361	2.849	3.556	4.107	4.837	5.422	6.011	7.425
810	13.500	2.370	2.860	3.570	4.125	4.860	5.450	6.045	7.475
815	13.583	2.380	2.872	3.585	4.142	4.881	5.474	6.073	7.512
820	13.667	2.390	2.884	3.599	4.160	4.902	5.498	6.100	7.548
825	13.750	2.400	2.896	3.614	4.177	4.923	5.523	6.128	7.585
830	13.833	2.410	2.908	3.629	4.195	4.944	5.547	6.155	7.622
835	13.917	2.420	2.920	3.644	4.213	4.966	5.571	6.183	7.658
840	14.000	2.430	2.932	3.658	4.230	4.987	5.595	6.210	7.695

Output Data to Export to PondPack, 5 minute intervals

Time (min)	Time (hours)	1 year (min)	2 year (min)	5 year (min)	10 year (min)	25 year (min)	50 year (min)	100 year (min)	500 year (min)
845	14.083	2.440	2.944	3.673	4.248	5.008	5.619	6.238	7.732
850	14.167	2.450	2.956	3.688	4.265	5.029	5.643	6.265	7.768
855	14.250	2.460	2.968	3.703	4.283	5.050	5.668	6.293	7.805
860	14.333	2.470	2.979	3.717	4.300	5.071	5.692	6.320	7.842
865	14.417	2.480	2.991	3.732	4.318	5.092	5.716	6.348	7.878
870	14.500	2.490	3.003	3.747	4.335	5.113	5.740	6.375	7.915
875	14.583	2.500	3.015	3.761	4.353	5.134	5.764	6.403	7.952
880	14.667	2.510	3.027	3.776	4.370	5.156	5.788	6.430	7.988
885	14.750	2.520	3.039	3.791	4.388	5.177	5.813	6.458	8.025
890	14.833	2.530	3.051	3.806	4.405	5.198	5.837	6.485	8.062
895	14.917	2.540	3.063	3.820	4.423	5.219	5.861	6.513	8.098
900	15.000	2.550	3.075	3.835	4.440	5.240	5.885	6.540	8.135
905	15.083	2.555	3.082	3.843	4.450	5.253	5.900	6.557	8.159
910	15.167	2.561	3.088	3.852	4.460	5.265	5.914	6.574	8.182
915	15.250	2.566	3.095	3.860	4.470	5.278	5.929	6.591	8.206
920	15.333	2.572	3.101	3.868	4.480	5.290	5.943	6.608	8.229
925	15.417	2.577	3.108	3.877	4.490	5.303	5.958	6.625	8.253
930	15.500	2.583	3.114	3.885	4.500	5.315	5.973	6.643	8.277
935	15.583	2.588	3.121	3.893	4.510	5.328	5.987	6.660	8.300
940	15.667	2.593	3.127	3.902	4.520	5.340	6.002	6.677	8.324
945	15.750	2.599	3.134	3.910	4.530	5.353	6.016	6.694	8.348
950	15.833	2.604	3.140	3.918	4.540	5.365	6.031	6.711	8.371
955	15.917	2.610	3.147	3.927	4.550	5.378	6.045	6.728	8.395
960	16.000	2.615	3.153	3.935	4.560	5.390	6.060	6.745	8.418
965	16.083	2.620	3.160	3.943	4.570	5.403	6.075	6.762	8.442
970	16.167	2.626	3.166	3.952	4.580	5.415	6.089	6.779	8.466
975	16.250	2.631	3.173	3.960	4.590	5.428	6.104	6.796	8.489
980	16.333	2.637	3.179	3.968	4.600	5.440	6.118	6.813	8.513
985	16.417	2.642	3.186	3.977	4.610	5.453	6.133	6.830	8.536
990	16.500	2.648	3.193	3.985	4.620	5.465	6.148	6.848	8.560
995	16.583	2.653	3.199	3.993	4.630	5.478	6.162	6.865	8.584
1000	16.667	2.658	3.206	4.002	4.640	5.490	6.177	6.882	8.607
1005	16.750	2.664	3.212	4.010	4.650	5.503	6.191	6.899	8.631
1010	16.833	2.669	3.219	4.018	4.660	5.515	6.206	6.916	8.654
1015	16.917	2.675	3.225	4.027	4.670	5.528	6.220	6.933	8.678
1020	17.000	2.680	3.232	4.035	4.680	5.540	6.235	6.950	8.702
1025	17.083	2.685	3.238	4.043	4.690	5.553	6.250	6.967	8.725
1030	17.167	2.691	3.245	4.052	4.700	5.565	6.264	6.984	8.749
1035	17.250	2.696	3.251	4.060	4.710	5.578	6.279	7.001	8.773
1040	17.333	2.702	3.258	4.068	4.720	5.590	6.293	7.018	8.796
1045	17.417	2.707	3.264	4.077	4.730	5.603	6.308	7.035	8.820
1050	17.500	2.713	3.271	4.085	4.740	5.615	6.323	7.053	8.843
1055	17.583	2.718	3.277	4.093	4.750	5.628	6.337	7.070	8.867
1060	17.667	2.723	3.284	4.102	4.760	5.640	6.352	7.087	8.891
1065	17.750	2.729	3.290	4.110	4.770	5.653	6.366	7.104	8.914
1070	17.833	2.734	3.297	4.118	4.780	5.665	6.381	7.121	8.938
1075	17.917	2.740	3.303	4.127	4.790	5.678	6.395	7.138	8.961
1080	18.000	2.745	3.310	4.135	4.800	5.690	6.410	7.155	8.985

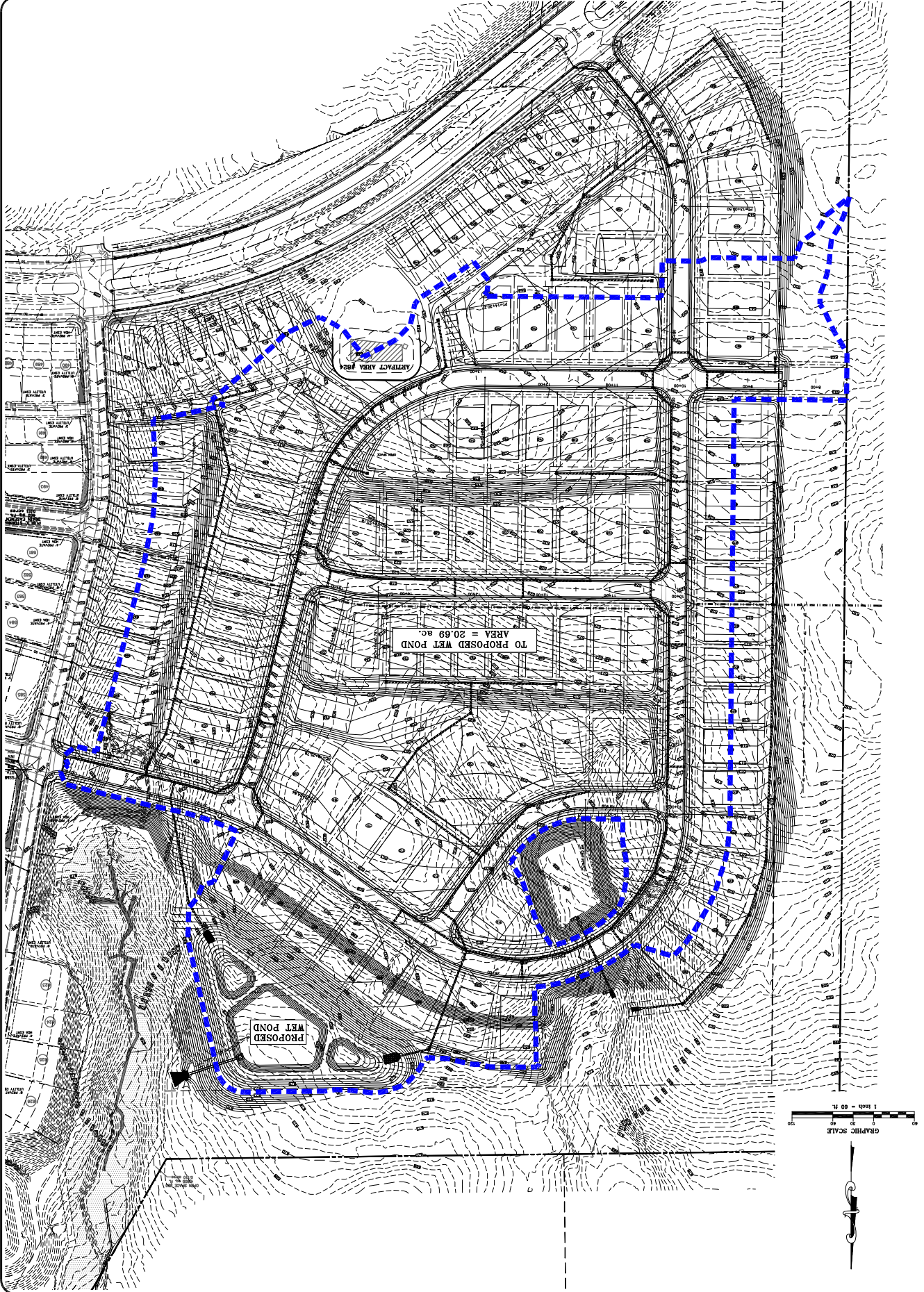
Output Data to Export to PondPack, 5 minute intervals

Time (min)	Time (hours)	1 year (min)	2 year (min)	5 year (min)	10 year (min)	25 year (min)	50 year (min)	100 year (min)	500 year (min)
1085	18.083	2.748	3.313	4.140	4.805	5.696	6.416	7.161	8.992
1090	18.167	2.751	3.317	4.144	4.810	5.701	6.422	7.168	8.999
1095	18.250	2.754	3.320	4.149	4.815	5.707	6.428	7.174	9.006
1100	18.333	2.756	3.324	4.153	4.820	5.713	6.434	7.181	9.013
1105	18.417	2.759	3.327	4.158	4.825	5.718	6.441	7.187	9.020
1110	18.500	2.762	3.331	4.162	4.830	5.724	6.447	7.194	9.027
1115	18.583	2.765	3.334	4.167	4.835	5.730	6.453	7.200	9.034
1120	18.667	2.768	3.338	4.171	4.840	5.736	6.459	7.207	9.041
1125	18.750	2.771	3.341	4.176	4.845	5.741	6.465	7.213	9.048
1130	18.833	2.773	3.345	4.180	4.850	5.747	6.471	7.220	9.055
1135	18.917	2.776	3.348	4.185	4.855	5.753	6.477	7.226	9.062
1140	19.000	2.779	3.352	4.189	4.860	5.758	6.483	7.233	9.069
1145	19.083	2.782	3.355	4.194	4.865	5.764	6.489	7.239	9.076
1150	19.167	2.785	3.359	4.198	4.870	5.770	6.496	7.245	9.083
1155	19.250	2.788	3.362	4.203	4.875	5.775	6.502	7.252	9.090
1160	19.333	2.791	3.366	4.207	4.880	5.781	6.508	7.258	9.097
1165	19.417	2.793	3.369	4.212	4.885	5.787	6.514	7.265	9.104
1170	19.500	2.796	3.373	4.216	4.890	5.793	6.520	7.271	9.111
1175	19.583	2.799	3.376	4.221	4.895	5.798	6.526	7.278	9.118
1180	19.667	2.802	3.379	4.225	4.900	5.804	6.532	7.284	9.125
1185	19.750	2.805	3.383	4.230	4.905	5.810	6.538	7.291	9.132
1190	19.833	2.808	3.386	4.234	4.910	5.815	6.544	7.297	9.139
1195	19.917	2.810	3.390	4.239	4.915	5.821	6.551	7.304	9.146
1200	20.000	2.813	3.393	4.243	4.920	5.827	6.557	7.310	9.153
1205	20.083	2.816	3.397	4.248	4.925	5.832	6.563	7.316	9.160
1210	20.167	2.819	3.400	4.252	4.930	5.838	6.569	7.323	9.167
1215	20.250	2.822	3.404	4.257	4.935	5.844	6.575	7.329	9.174
1220	20.333	2.825	3.407	4.261	4.940	5.849	6.581	7.336	9.181
1225	20.417	2.828	3.411	4.266	4.945	5.855	6.587	7.342	9.188
1230	20.500	2.830	3.414	4.270	4.950	5.861	6.593	7.349	9.195
1235	20.583	2.833	3.418	4.275	4.955	5.867	6.599	7.355	9.202
1240	20.667	2.836	3.421	4.279	4.960	5.872	6.606	7.362	9.209
1245	20.750	2.839	3.425	4.284	4.965	5.878	6.612	7.368	9.216
1250	20.833	2.842	3.428	4.288	4.970	5.884	6.618	7.375	9.223
1255	20.917	2.845	3.432	4.293	4.975	5.889	6.624	7.381	9.230
1260	21.000	2.848	3.435	4.298	4.980	5.895	6.630	7.388	9.238
1265	21.083	2.850	3.438	4.302	4.985	5.901	6.636	7.394	9.245
1270	21.167	2.853	3.442	4.307	4.990	5.906	6.642	7.400	9.252
1275	21.250	2.856	3.445	4.311	4.995	5.912	6.648	7.407	9.259
1280	21.333	2.859	3.449	4.316	5.000	5.918	6.654	7.413	9.266
1285	21.417	2.862	3.452	4.320	5.005	5.923	6.661	7.420	9.273
1290	21.500	2.865	3.456	4.325	5.010	5.929	6.667	7.426	9.280
1295	21.583	2.867	3.459	4.329	5.015	5.935	6.673	7.433	9.287
1300	21.667	2.870	3.463	4.334	5.020	5.941	6.679	7.439	9.294
1305	21.750	2.873	3.466	4.338	5.025	5.946	6.685	7.446	9.301
1310	21.833	2.876	3.470	4.343	5.030	5.952	6.691	7.452	9.308
1315	21.917	2.879	3.473	4.347	5.035	5.958	6.697	7.459	9.315
1320	22.000	2.882	3.477	4.352	5.040	5.963	6.703	7.465	9.322

Output Data to Export to PondPack, 5 minute intervals

Time (min)	Time (hours)	1 year (min)	2 year (min)	5 year (min)	10 year (min)	25 year (min)	50 year (min)	100 year (min)	500 year (min)
1325	22.083	2.885	3.480	4.356	5.045	5.969	6.709	7.471	9.329
1330	22.167	2.887	3.484	4.361	5.050	5.975	6.716	7.478	9.336
1335	22.250	2.890	3.487	4.365	5.055	5.980	6.722	7.484	9.343
1340	22.333	2.893	3.491	4.370	5.060	5.986	6.728	7.491	9.350
1345	22.417	2.896	3.494	4.374	5.065	5.992	6.734	7.497	9.357
1350	22.500	2.899	3.498	4.379	5.070	5.998	6.740	7.504	9.364
1355	22.583	2.902	3.501	4.383	5.075	6.003	6.746	7.510	9.371
1360	22.667	2.904	3.504	4.388	5.080	6.009	6.752	7.517	9.378
1365	22.750	2.907	3.508	4.392	5.085	6.015	6.758	7.523	9.385
1370	22.833	2.910	3.511	4.397	5.090	6.020	6.764	7.530	9.392
1375	22.917	2.913	3.515	4.401	5.095	6.026	6.771	7.536	9.399
1380	23.000	2.916	3.518	4.406	5.100	6.032	6.777	7.543	9.406
1385	23.083	2.919	3.522	4.410	5.105	6.037	6.783	7.549	9.413
1390	23.167	2.922	3.525	4.415	5.110	6.043	6.789	7.555	9.420
1395	23.250	2.924	3.529	4.419	5.115	6.049	6.795	7.562	9.427
1400	23.333	2.927	3.532	4.424	5.120	6.054	6.801	7.568	9.434
1405	23.417	2.930	3.536	4.428	5.125	6.060	6.807	7.575	9.441
1410	23.500	2.933	3.539	4.433	5.130	6.066	6.813	7.581	9.448
1415	23.583	2.936	3.543	4.437	5.135	6.072	6.819	7.588	9.455
1420	23.667	2.939	3.546	4.442	5.140	6.077	6.826	7.594	9.462
1425	23.750	2.941	3.550	4.446	5.145	6.083	6.832	7.601	9.469
1430	23.833	2.944	3.553	4.451	5.150	6.089	6.838	7.607	9.476
1435	23.917	2.947	3.557	4.455	5.155	6.094	6.844	7.614	9.483
1440	24.000	2.950	3.560	4.460	5.160	6.100	6.850	7.620	9.490

HYDROLOGIC CALCULATIONS



HYDROLOGIC CALCULATIONS
Post-Development-To Wet Pond

I. SCS CURVE NUMBERS

HSG	Impervious	Open	Wooded
A	98	39	30
B	98	61	55
C	98	74	70
D	98	80	77

Assume:

HSG 'A' =	0.0%
HSG 'B' =	100.0%
HSG 'C' =	0.0%
HSG 'D' =	0.0%

Cover Condition	SCS CN	Comments
Impervious	98	-
Open	61	Assume good condition
Wooded	55	Assume good condition
Water	100	-

II. POST-DEVELOPMENT

=> To Wet Pond

A. Watershed Breakdown

Total Number of Single-Family 50' Lots =	37	lots
Assumed Impervious Area Per Single-Family 50' Lot =	3,500	square feet
Total Impervious Area from Single-Family 50' Lots =	129,500	square feet
=	2.97	acres
Total Number of Single-Family 60' Lots =	23.25	lots
Assumed Impervious Area Per Single-Family 60' Lot =	3,800	square feet
Total Impervious Area from Single-Family 60' Lots =	88,350	square feet
=	2.03	acres
Total Number of Single-Family 50' Corner Lots =	11	lots
Assumed Impervious Area Per Single-Family 50' Corner Lot =	3,700	square feet
Total Impervious Area from Single-Family 50' Corner Lots =	40,700	square feet
=	0.93	acres
Total Number of Single-Family 60' Corner Lots =	5.5	lots
Assumed Impervious Area Per Single-Family 60' Corner Lot =	4,000	square feet
Total Impervious Area from Single-Family 60' Corner Lots =	22,000	square feet
=	0.51	acres
Total Open Space Lots =	2	lots
Assumed Impervious Area Per Open Space Lot =	5,000	square feet
Total Impervious Area from Open Space Lots =	10,000	square feet
=	0.23	acres
Total Sidewalk Impervious Area =	32,704	square feet
=	0.75	acres
Total Roadway Impervious Area =	123,537	square feet
=	2.84	acres

HYDROLOGIC CALCULATIONS
Post-Development-To Wet Pond

Contributing Area	SCS CN	Area [acres]	Comments
On-site open	61	9.84	Assume good condition
On-site impervious	98	10.26	-
On-site wooded	55	0.00	Assume good condition
On-site pond	100	0.59	-
Off-site open	61	0.00	Assume good condition
Off-site impervious	98	0.00	-
Off-site wooded	55	0.00	Assume good condition
Off-site pond	100	0.00	-

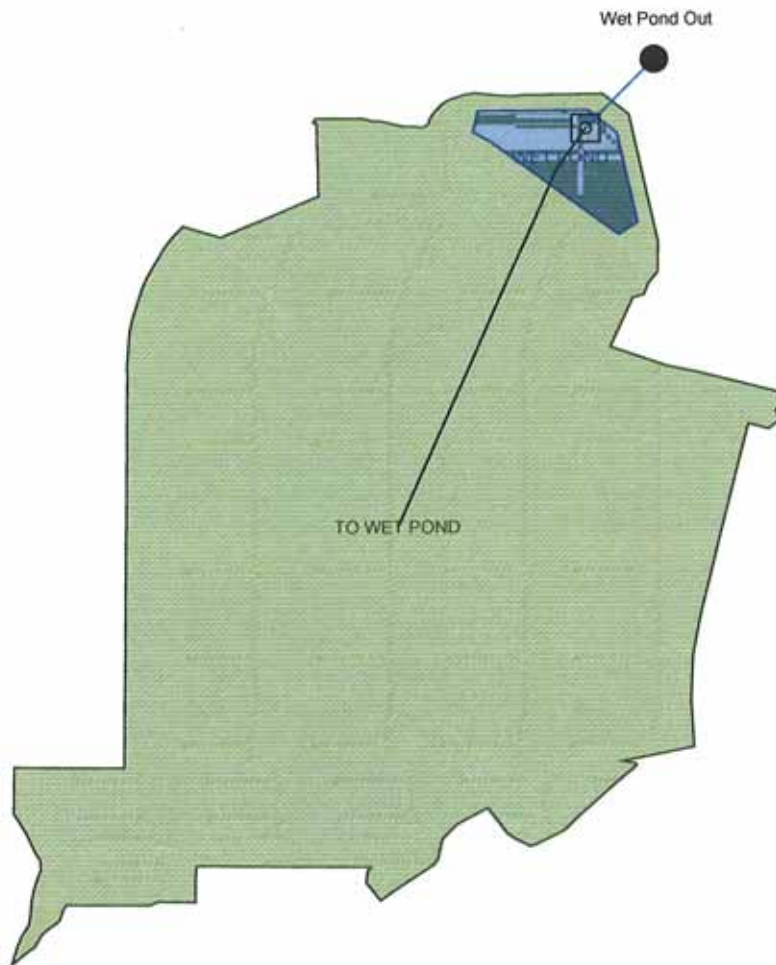
Total area = 20.69 acres
0.0323 sq.mi.
Composite SCS CN = 80
% Impervious = 49.6%

B. Time of Concentration Information

Due to the amount of piped and overland pavement flow, the post-development time of concentration was assumed to be 5 minute

Time of Concentration =	5.00	minutes
SCS Lag Time =	3.00	minutes (SCS Lag = 0.6* Tc)
	= 0.0500	hours
Time Increment =	0.87	minutes (= 0.29*SCS Lag)

Scenario: Post



Subsection: Master Network Summary

Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ft ³)	Time to Peak (min)	Peak Flow (ft ³ /s)
TO WET POND	Post-1	1	90,942.000	722.000	43.46
TO WET POND	Post-2	2	126,338.000	721.000	60.48
TO WET POND	Post-10	10	227,527.000	721.000	96.67
TO WET POND	Post-25	25	290,462.000	721.000	114.39
TO WET POND	Post-100	100	395,443.000	721.000	138.31

Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ft ³)	Time to Peak (min)	Peak Flow (ft ³ /s)
Wet Pond Out	Post-1	1	14,621.000	1,440.000	0.36
Wet Pond Out	Post-2	2	45,610.000	901.000	2.20
Wet Pond Out	Post-10	10	146,061.000	751.000	24.41
Wet Pond Out	Post-25	25	208,656.000	729.000	50.33
Wet Pond Out	Post-100	100	313,207.000	728.000	70.98

Pond Summary

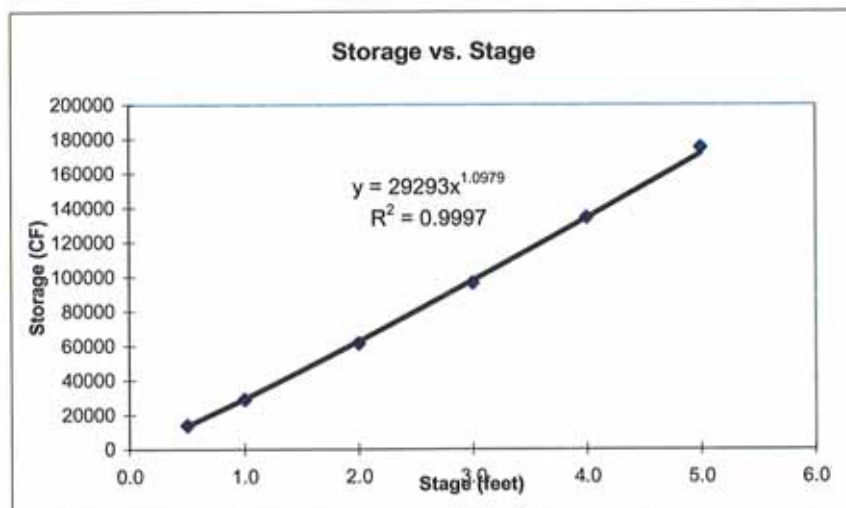
Label	Scenario	Return Event (years)	Hydrograph Volume (ft ³)	Time to Peak (min)	Peak Flow (ft ³ /s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ft ³)
WET POND (IN)	Post-1	1	90,942.000	722.000	43.46	(N/A)	(N/A)
WET POND (OUT)	Post-1	1	14,621.000	1,440.000	0.36	474.39	76,322.000
WET POND (IN)	Post-2	2	126,338.000	721.000	60.48	(N/A)	(N/A)
WET POND (OUT)	Post-2	2	45,610.000	901.000	2.20	474.60	83,510.000
WET POND (IN)	Post-10	10	227,527.000	721.000	96.67	(N/A)	(N/A)
WET POND (OUT)	Post-10	10	146,061.000	751.000	24.41	475.04	99,361.000
WET POND (IN)	Post-25	25	290,462.000	721.000	114.39	(N/A)	(N/A)
WET POND (OUT)	Post-25	25	208,656.000	729.000	50.33	475.38	111,706.000
WET POND (IN)	Post-100	100	395,443.000	721.000	138.31	(N/A)	(N/A)
WET POND (OUT)	Post-100	100	313,207.000	728.000	70.98	475.94	131,884.000

WET POND FINAL DESIGN CALCULATIONS

Stage-Storage Function

Project Name: Briar Chapel - Phase 6 North
Designer: J. Finch, PE
Job Number: NEW-12000
Date: 5/10/2012

Contour (feet)	Stage (feet)	Contour Area (SF)	Average Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	Estimated Volume w/ S-S Fxn (CF)
472.00	0.0	25,869				
472.50	0.5	29,691	27780	13890	13890	0.51
473.00	1.0	31,131	30411	15206	29096	0.99
474.00	2.0	33,737	32434	32434	61529	1.97
475.00	3.0	36,442	35089	35089	96619	2.97
476.00	4.0	39,246	37844	37844	134462	4.01
477.00	5.0	42,150	40698	40698	175160	5.10



Ks =	29293
b =	1.0979

WET POND

==> *Stage - Storage Function*

Ks = 29293

b = 1.0979

Zo = 472.00

Elevation [feet]	Storage	
	[cf]	[acre-feet]
472.00	0	0.000
472.20	5005	0.115
472.40	10712	0.246
472.60	16718	0.384
472.80	22928	0.526
473.00	29293	0.672
473.20	35785	0.822
473.40	42384	0.973
473.60	49076	1.127
473.80	55851	1.282
474.00	62700	1.439
474.20	69616	1.598
474.40	76595	1.758
474.60	83630	1.920
474.80	90719	2.083
475.00	97858	2.247
475.20	105043	2.411
475.40	112273	2.577
475.60	119544	2.744
475.80	126855	2.912
476.00	134204	3.081
476.20	141589	3.250
476.40	149008	3.421
476.60	156461	3.592
476.80	163945	3.764
477.00	171460	3.936

Subsection: Outlet Input Data

Label: Wet Pond

Requested Pond Water Surface Elevations

Minimum (Headwater)	472.00 ft
Increment (Headwater)	0.10 ft
Maximum (Headwater)	477.00 ft

Outlet Connectivity

Structure Type	Outlet ID	Direction	Outfall	E1 (ft)	E2 (ft)
Inlet Box	Riser - 1	Forward	Culvert - 1	474.50	477.00
Orifice-Circular	Orifice - 1	Forward	Culvert - 1	472.00	477.00
Culvert-Circular	Culvert - 1	Forward	TW	466.00	477.00
Tailwater Settings	Tailwater			(N/A)	(N/A)

Subsection: Outlet Input Data

Label: Wet Pond

Structure ID: Riser - 1	
Structure Type: Inlet Box	
Number of Openings	1
Elevation	474.50 ft
Orifice Area	25.0 ft ²
Orifice Coefficient	0.600
Weir Length	20.00 ft
Weir Coefficient	3.00 (ft ^{0.5})/s
K Reverse	1.000
Manning's n	0.000
Kev, Charged Riser	0.000
Weir Submergence	False
Orifice H to crest	False

Subsection: Outlet Input Data

Label: Wet Pond

Structure ID: Culvert - 1	
Structure Type: Culvert-Circular	
Number of Barrels	1
Diameter	30.0 in
Length	83.00 ft
Length (Computed Barrel)	83.10 ft
Slope (Computed)	0.048 ft/ft
Outlet Control Data	
Manning's n	0.013
Ke	0.500
Kb	0.009
Kr	0.000
Convergence Tolerance	0.00 ft
Inlet Control Data	
Equation Form	Form 1
K	0.0098
M	2.0000
C	0.0398
Y	0.6700
T1 ratio (HW/D)	0.000
T2 ratio (HW/D)	1.283
Slope Correction Factor	-0.500

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

T1 Elevation	466.00 ft	T1 Flow	27.16 ft ³ /s
T2 Elevation	469.21 ft	T2 Flow	31.05 ft ³ /s

Subsection: Outlet Input Data

Label: Wet Pond

Structure ID: Orifice - 1	
Structure Type: Orifice-Circular	
Number of Openings	1
Elevation	472.00 ft
Orifice Diameter	3.0 in
Orifice Coefficient	0.600
Structure ID: TW	
Structure Type: TW Setup, DS Channel	
Tailwater Type	Free Outfall
Convergence Tolerances	
Maximum Iterations	30
Tailwater Tolerance (Minimum)	0.01 ft
Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft
Headwater Tolerance (Maximum)	0.50 ft
Flow Tolerance (Minimum)	0.001 ft ³ /s
Flow Tolerance (Maximum)	10.000 ft ³ /s

Subsection: Composite Rating Curve

Label: Wet Pond

Composite Outflow Summary

Water Surface Elevation (ft)	Flow (ft ³ /s)	Tailwater Elevation (ft)	Convergence Error (ft)
472.00	0.00	(N/A)	0.00
472.10	0.02	(N/A)	0.00
472.20	0.06	(N/A)	0.00
472.30	0.10	(N/A)	0.00
472.40	0.12	(N/A)	0.00
472.50	0.14	(N/A)	0.00
472.60	0.16	(N/A)	0.00
472.70	0.18	(N/A)	0.00
472.80	0.19	(N/A)	0.00
472.90	0.21	(N/A)	0.00
473.00	0.22	(N/A)	0.00
473.10	0.23	(N/A)	0.00
473.20	0.25	(N/A)	0.00
473.30	0.26	(N/A)	0.00
473.40	0.27	(N/A)	0.00
473.50	0.28	(N/A)	0.00
473.60	0.29	(N/A)	0.00
473.70	0.30	(N/A)	0.00
473.80	0.30	(N/A)	0.00
473.90	0.31	(N/A)	0.00
474.00	0.32	(N/A)	0.00
474.10	0.33	(N/A)	0.00
474.20	0.34	(N/A)	0.00
474.30	0.35	(N/A)	0.00
474.40	0.36	(N/A)	0.00
474.50	0.37	(N/A)	0.00
474.60	2.27	(N/A)	0.00
474.70	5.74	(N/A)	0.00
474.80	10.25	(N/A)	0.00
474.90	15.57	(N/A)	0.00
475.00	21.62	(N/A)	0.00
475.10	28.29	(N/A)	0.00
475.20	35.55	(N/A)	0.00
475.30	43.36	(N/A)	0.00
475.40	51.63	(N/A)	0.00
475.50	60.31	(N/A)	0.00
475.60	69.26	(N/A)	0.00
475.70	69.96	(N/A)	0.00
475.80	70.39	(N/A)	0.00
475.90	70.82	(N/A)	0.00
476.00	71.25	(N/A)	0.00



A division of The John R. McAdams Company, Inc.

Label: Wet Pond

Water Surface

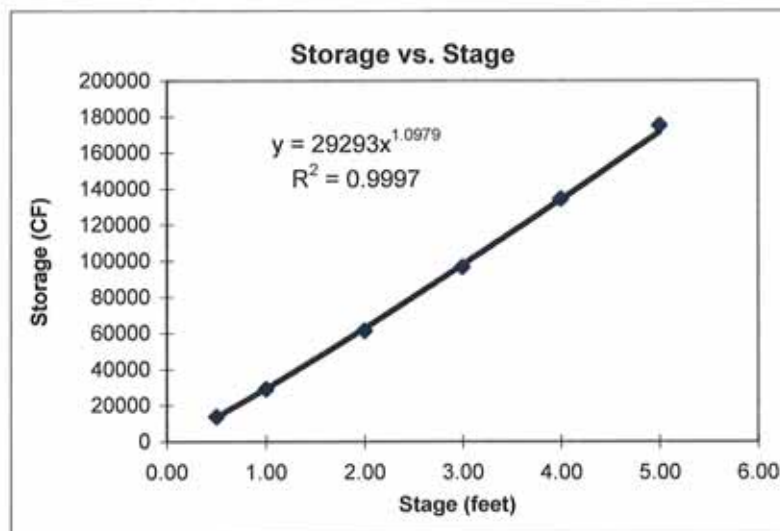
Water Surface Elevation (ft)	Flow (ft ³ /s)	Tailwater Elevation (ft)	Convergence Error (ft)
476.10	71.67	(N/A)	0.00
476.20	72.10	(N/A)	0.00
476.30	72.52	(N/A)	0.00
476.40	72.93	(N/A)	0.00
476.50	73.34	(N/A)	0.00
476.60	73.75	(N/A)	0.00
476.70	74.17	(N/A)	0.00
476.80	74.57	(N/A)	0.00
476.90	74.98	(N/A)	0.00
477.00	75.38	(N/A)	0.00

Contributing Structures

(no Q: Riser - 1,Orifice - 1,Culvert - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
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Orifice - 1,Culvert - 1 (no Q: Riser - 1)
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Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Orifice - 1,Culvert - 1 (no Q: Riser - 1)
Riser - 1,Orifice - 1,Culvert - 1
Riser - 1,Orifice - 1,Culvert - 1
Riser - 1,Orifice - 1,Culvert - 1
Riser - 1,Orifice - 1,Culvert - 1

STAGE-STORAGE FUNCTION - ABOVE NORMAL POOL

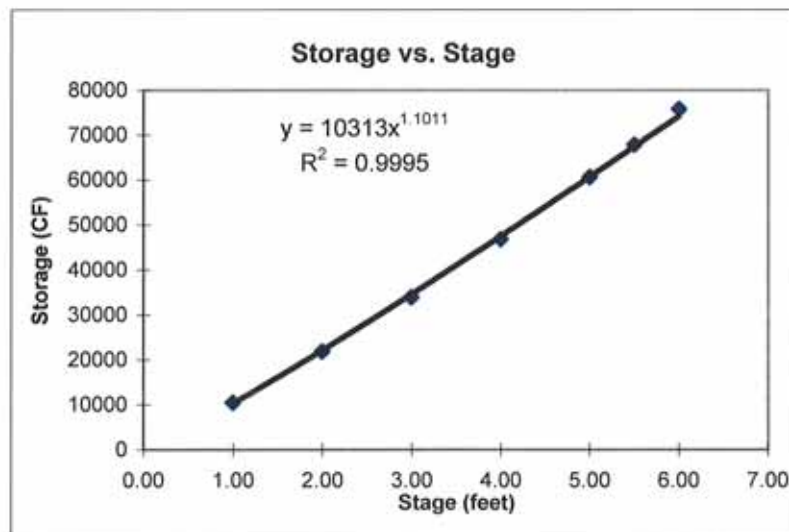
Contour (feet)	Stage (feet)	Contour Area (SF)	Average Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	Estimated Stage w/ S-S Fxn (feet)
472.00	0.00	25,869				
472.50	0.50	29,691	27780	13890	13890	0.51
473.00	1.00	31,131	30411	15206	29096	0.99
474.00	2.00	33,737	32434	32434	61529	1.97
475.00	3.00	36,442	35089	35089	96619	2.97
476.00	4.00	39,246	37844	37844	134462	4.01
477.00	5.00	42,150	40698	40698	175160	5.10



$K_s =$	29293
$b =$	1.0979

STAGE-STORAGE FUNCTION - MAIN POOL

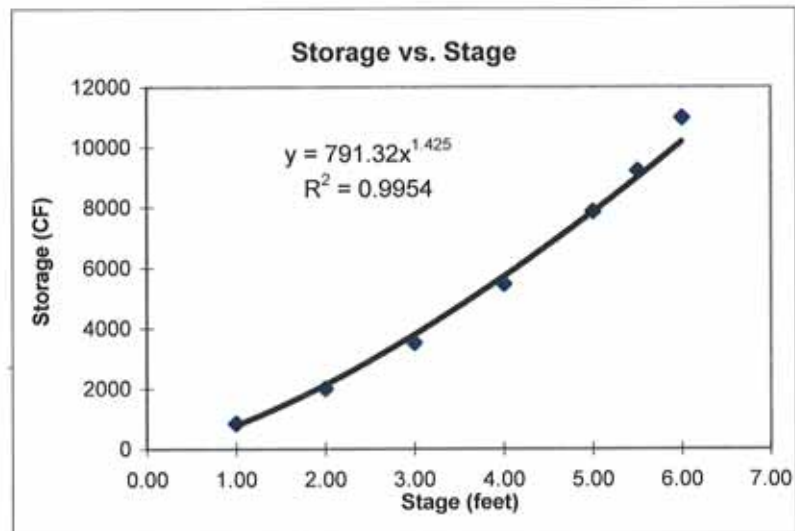
Contour (feet)	Stage (feet)	Contour Area (SF)	Average Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	Estimated Stage w/ S-S Fxn (feet)
466.00	0.00	10,127				
467.00	1.00	10,897	10512	10512	10512	1.02
468.00	2.00	11,692	11294	11294	21806	1.97
469.00	3.00	12,512	12102	12102	33907	2.95
470.00	4.00	13,357	12934	12934	46842	3.95
471.00	5.00	14,227	13792	13792	60633	5.00
471.50	5.50	14,672	14449	7225	67858	5.53
472.00	6.00	17,128	15900	7950	75808	6.12



$K_s =$	10313
$b =$	1.1011

STAGE-STORAGE FUNCTION - NORTH FOREBAY

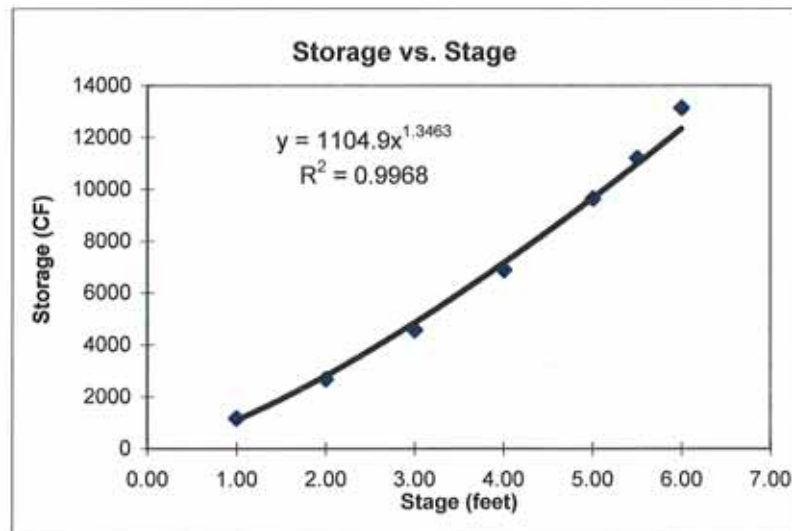
Contour (feet)	Stage (feet)	Contour Area (SF)	Average Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	Estimated Stage w/ S-S Fxn (feet)
466.00	0.00	744				
467.00	1.00	963	853	853	853	1.05
468.00	2.00	1,320	1142	1142	1995	1.91
469.00	3.00	1,724	1522	1522	3517	2.85
470.00	4.00	2,174	1949	1949	5466	3.88
471.00	5.00	2,615	2395	2395	7861	5.01
471.50	5.50	2,821	2718	1359	9220	5.60
472.00	6.00	4,156	3488	1744	10964	6.33



$K_s =$	791.32
$b =$	1.4250

STAGE-STORAGE FUNCTION - NORTH FOREBAY

Contour (feet)	Stage (feet)	Contour Area (SF)	Average Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	Estimated Stage w/ S-S Fxn (feet)
460.00	0.00	1,009				
461.00	1.00	1,333	1171	1171	1171	1.04
462.00	2.00	1,693	1513	1513	2684	1.93
463.00	3.00	2,090	1891	1891	4575	2.87
464.00	4.00	2,524	2307	2307	6882	3.89
465.00	5.00	2,994	2759	2759	9641	5.00
465.50	5.50	3,207	3100	1550	11191	5.58
466.00	6.00	4,586	3896	1948	13139	6.29



$K_s =$	1104.9
$b =$	1.3463

I. TOTAL VOLUME OF FACILITY

Volume of Main Pool =	75,808	cf
Volume of Forebay #1 =	10,964	cf
Volume of Forebay #2 =	13,139	cf
Total Volume Below NWSE =	99,911	cf
	= 2.29	acre-ft
Total Volume Above NWSE =	175,160	cf
	= 4.02	acre-ft
Total Volume of Facility =	275,071	cf
	= 6.31	acre-ft

II. FOREBAY PERCENTAGE OF PERMANENT POOL VOLUME

Per NCDWQ design guidelines, the forebay volume should equal approximately 20% of the total permanent pool volume.

Total Volume Below NWSE =	99,911	cf
Volume of Forebay #1 =	10,964	cf
Volume of Forebay #2 =	13,139	cf
Total Volume of Forebays =	24,103	cf
% Forebay =	24.1%	

III. AVERAGE DEPTH OF POND

Total Volume Below NWSE =	99,911	cf
Surface Area at NWSE =	25,869	sf
Average Depth =	3.86	ft

Table 10-3

Surface Area to Drainage Area Ratio for Permanent Pool Sizing to Achieve 90 Percent TSS Pollutant Removal Efficiency in the Mountain and Piedmont Regions, Adapted from Driscoll, 1986

Percent Impervious Cover	Permanent Pool Average Depth (ft)												
	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0
10%	0.9	0.8	0.8	0.7	0.6	0.6	0.5	0.5	0.5	0.5	0.4	0.4	0.4
20%	1.5	1.3	1.1	1.0	1.0	0.9	0.9	0.9	0.8	0.8	0.8	0.7	0.7
30%	1.9	1.8	1.7	1.5	1.4	1.4	1.3	1.1	1.0	1.0	1.0	0.9	0.9
40%	2.5	2.3	2.0	1.9	1.8	1.7	1.6	1.6	1.5	1.4	1.3	1.2	1.1
50%	3.0	2.8	2.5	2.3	2.0	1.9	1.9	1.8	1.7	1.6	1.6	1.5	1.5
60%	3.5	3.2	2.8	2.7	2.5	2.4	2.2	2.1	1.9	1.9	1.8	1.8	1.7
70%	4.0	3.7	3.3	3.1	2.8	2.7	2.5	2.4	2.2	2.1	2.0	2.0	1.9
80%	4.5	4.1	3.8	3.5	3.3	3.0	2.8	2.7	2.6	2.4	2.3	2.1	2.0
90%	5.0	4.5	4.0	3.8	3.5	3.3	3.0	2.9	2.8	2.7	2.6	2.5	2.4

Table 10-4

Surface Area to Drainage Area Ratio for Permanent Pool Sizing to Achieve 90 Percent TSS Pollutant Removal Efficiency in the Coastal Region, Adapted from Driscoll, 1986

Percent Impervious Cover	Permanent Pool Average Depth (ft)									
	3.0	3.5	4.0	4.5	5.0	5.5	6.0	6.5	7.0	7.5'
10%	1.3	1.0	0.8	0.7	0.6	0.5	0.4	0.3	0.2	0.1
20%	2.4	2.0	1.8	1.7	1.5	1.4	1.2	1.0	0.9	0.6
30%	3.5	3.0	2.7	2.5	2.2	1.9	1.6	1.3	1.1	0.8
40%	4.5	4.0	3.5	3.1	2.8	2.5	2.1	1.8	1.4	1.1
50%	5.6	5.0	4.3	3.9	3.5	3.1	2.7	2.3	1.9	1.5
60%	7.0	6.0	5.3	4.8	4.3	3.9	3.4	2.9	2.4	1.9
70%	8.1	7.0	6.0	5.5	5.0	4.5	3.9	3.4	2.9	2.3
80%	9.4	8.0	7.0	6.4	5.7	5.2	4.6	4.0	3.4	2.8
90%	10.7	9.0	7.9	7.2	6.5	5.9	5.2	4.6	3.9	3.3
100%	12	10.0	8.8	8.1	7.3	6.6	5.8	5.1	4.3	3.6

The engineering design of a wet detention basin must include a 10-foot-wide (minimum) vegetated shelf around the full perimeter of the basin. The inside edge of the shelf shall be no deeper than 6" below the permanent pool level, and the outside edge shall be 6" above the permanent pool level. For a 10' wide shelf, the resulting slope is 10:1. With half the required shelf below the water (maximum depth of 6 inches), and half the required shelf above the water, the vegetated shelf will provide a location for a diverse population of emergent wetland vegetation that enhances biological pollutant removal, provides a habitat for wildlife, protects the shoreline from erosion, and improves sediment trap efficiency. A 10' wide shelf also provides a safety feature prior to the deeper permanent pool.

Short-circuiting of the stormwater must be prevented. The most direct way of minimizing short-circuiting is to maximize the length of the flow path between the inlet and the outlet: basins with long and narrow shapes can maximize the length of the flow path. Long and narrow but irregularly shaped wet detention basins may appear more

WET DETENTION POND
Surface Area Calculation

WET DETENTION BASIN SUMMARY

From *Stormwater Best Management Practices Manual*. NCDENR: Division of Water Quality, October 2007.

Enter the drainage area characteristics ==>

Total drainage area to pond = 20.69 acres
Total impervious area to pond = 10.26 acres

Note The basin must be sized to treat all impervious surface runoff draining into the pond, not just the impervious surface from on-site development.

Drainage area = 20.69 acres @ 49.6% impervious

Estimate the surface area required at pond normal pool elevation ==>

Wet Detention Basins are based on an minimum average depth of = 3.86 feet (*Calculated*)

From the DWQ BMP Handbook (10/2007), the required SA/DA ratio for 90% TSS Removal ==>

		3.5	3.86	4.0
Lower Boundary =>	40.0	2.3		2.0
Site % impervious =>	49.6	2.78	2.56	2.5
Upper Boundary =>	50.0	2.8		2.5

Therefore, SA/DA required = 2.56

Surface area required at normal pool = 23,085 ft²
= 0.53 acres
Surface area provided at normal pool = 25,869 ft²

WATER QUALITY VOLUME CALCULATIONS

==> Determination of Water Quality Volume (1" Rainfall Depth)

Proposed Conditions ==>

$$WQ_v = (P)(R_v)(A)/12$$

where,

WQ_v = water quality volume (in acre-ft)

R_v = 0.05+0.009(I) where I is percent impervious cover

A = area in acres

P = rainfall (in inches)

Input data:

Total area, A = 20.69 acres
= 901,122 sf
Impervious area = 10.26 acres
= 446,791 sf
Percent impervious cover, I = 49.6 %
Rainfall, P = 1.0 inches

Calculated values:

R_v = 0.50
WQ_v = 0.855 acre-ft
= 37,264 cf.

==> Associated Depth above Wet Pond Permanent Pool

Ks = 29293
b = 1.0979
V = 37264
Normal Pool Elevation = 472.00 feet
Riser Crest Elevation = 474.50 feet

WQ Elevation = 473.25 feet

Inverted Siphon Design Sheet

D orifice = 3 inch
 # orifices = 1
 Ks = 29293
 b = 1.0979
 Cd siphon = 0.60
 Normal Pool Elevation = 473.00 feet
 Volume @ Normal Pool = 0 cf
 Orifice Invert = 473.00 feet
 WSEL @ 1" Runoff Volume = 474.25 feet

WSEL (feet)	Vol. Stored (cf)	Siphon Flow (cfs)	Avg. Flow (cfs)	Incr. Vol. (cf)	Incr. Time (sec)
474.25	37264	0.250			
474.14	33691	0.237	0.244	3573	14673
474.03	30152	0.224	0.231	3539	15344
473.92	26649	0.210	0.217	3503	16136
473.81	23187	0.195	0.203	3462	17092
473.70	19770	0.179	0.187	3416	18278
473.59	16406	0.161	0.170	3364	19810
473.48	13102	0.141	0.151	3304	21908
473.37	9872	0.117	0.129	3230	25057
473.26	6735	0.087	0.102	3137	30683
473.15	3726.4	0.040	0.064	3008	47222

Drawdown Time = 2.62 days

By comparison, if calculated by the average head over the orifice (assuming average head is one-third the total depth), the result would be:

Average driving head on orifice = 0.373 feet
 Orifice composite loss coefficient = 0.600
 Cross-sectional area of 3" orifice = 0.049 sf

Q = 0.1444 cfs

Drawdown Time = Volume / Flowrate / 86400 (sec/day)

Drawdown Time = 2.99 days

Conclusion : Use 1 - 3" Diameter Inverted Siphon to drawdown the accumulated volume from the 1.0" storm runoff, with a required time of about 2.62 days.

Square Riser/Barrel Anti-Flotation Calculation Sheet

Input Data ==>

Inside length of riser =	5.00 feet	
Inside width of riser =	5.00 feet	
Wall thickness of riser =	6.00 inches	
Base thickness of riser =	8.00 inches	
Base length of riser =	6.00 feet	
Base width of riser =	6.00 feet	
Inside height of Riser =	8.50 feet	
Concrete unit weight =	142.0 PCF	<i>Note: NC Products lists unit wt. of</i>
OD of barrel exiting manhole =	44.00 inches	<i>manhole concrete at 142 PCF.</i>
Size of drain pipe (if present) =	8.0 inches	
Trash Rack water displacement =	61.74 CF	

Concrete Present in Riser Structure ==>

Total amount of concrete:

Base of Riser =	24.000 CF
Riser Walls =	93.500 CF

Adjust for openings:

Opening for barrel =	5.280 CF
Opening for drain pipe =	0.175 CF

Total Concrete present, adjusted for openings =	112.046 CF
Weight of concrete present =	15911 lbs

Amount of water displaced by Riser Structure ==>

Displacement by concrete =	112.046 CF
Displacement by open air in riser =	212.500 CF
Displacement by trash rack =	61.740 CF

Total water displaced by riser/barrel structure =	386.286 CF
Weight of water displaced =	24104 lbs

Calculate amount of concrete to be added to riser ==>

Safety factor to use =	1.25 (recommend 1.25 or higher)
Must add =	14220 lbs concrete for buoyancy

Concrete unit weight for use =	142 PCF (note above observation for NCP concrete)
Buoyant weight of this concrete =	79.60 PCF
Buoyant, with safety factor applied =	63.68 PCF

Therefore, must add = 223.301 CF of concrete

Standard based described above = 24.000 CF of concrete

Therefore, base design must have = 247.301 CF of concrete

Calculate size of base for riser assembly ==>

Length = 9.000 feet
Width = 9.000 feet
Thickness = 37.0 inches

Concrete Present = 249.750 CF **OK**

Check validity of base as designed ==>

Total Water Displaced = 612.036 CF
Total Concrete Present = 337.796 CF

Total Water Displaced = 38191 lbs
Total Concrete Present = 47967 lbs

Actual safety factor = 1.26 **OK**

Results of design ==>

Base length =	9.00 feet
Base width =	9.00 feet
Base Thickness =	37.00 inches
CY of concrete total in base =	9.25 CY
Concrete unit weight in added base >=	142 PCF

Briar Chapel – Phase 6 North

Project # NEW-12000

VELOCITY DISSIPATOR DESIGN

Designed By: J. Finch, PE

Velocity Dissipator – Proposed Wet Pond

NRCD Land Quality Section Pipe Design

Entering the following values will provide you with the expected outlet velocity and depth of flow in a pipe, assuming the Mannings roughness number is constant over the entire length of the pipe.

flow Q in cfs : 25 Flow depth (ft) = 0.90
slope S in % : 4.82 Outlet velocity (fps) = 15.698
pipe diameter D in in. : 30
Manning number n : 0.013

NRCD Land Quality Section NYDOT Dissipator Design Results

Pipe diameter (ft) 2.50
Outlet velocity (fps) 15.70
Apron length (ft) 20.00

AVG DIAM (inches)	STONE CLASS	THICKNESS (inches)
-----	-----	-----
3	A	9
6	B	22
» 13	B or 1	22 «
23	2	27

Width Calculation

WIDTH = La + Do
WIDTH = 20 + 2.5
WIDTH = 23 FEET

CONCLUSION

Use NCDOT Class '1' Rip Rap
20'L x 23'W x 22"Thick